

Numerical Study of the Self-ignition of Tetrafluoroethylene in a 100-dm³-reactor

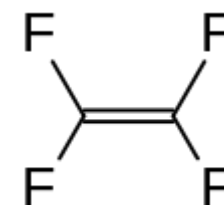
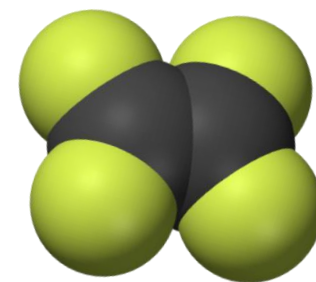
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What is tetrafluoroethylene (TFE)?

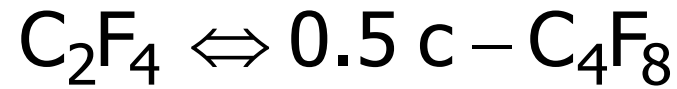
- Tetrafluoroethylene (C_2F_4) is a colorless gas
- TFE has a wide commercial relevance
 - PTFE (Teflon®)
 - PTFE Co-polymers
- TFE is a chemically unstable gas → explosive decomposition without oxidant (accidents in chemical plants*)
- Focus: ignition of TFE caused by contact on hot surfaces (self-ignition)



Main reactions

TFE at high pressure comes in contact with hot surfaces

DIMERIZATION 

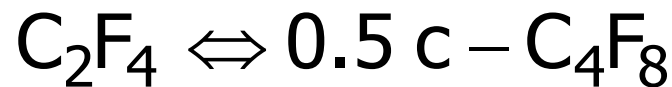


$$\Delta H_R = -103(\text{kJ}/\text{mol}_{\text{TFE}})$$

Main reactions

TFE at high pressure comes in contact with hot surfaces

DIMERIZATION



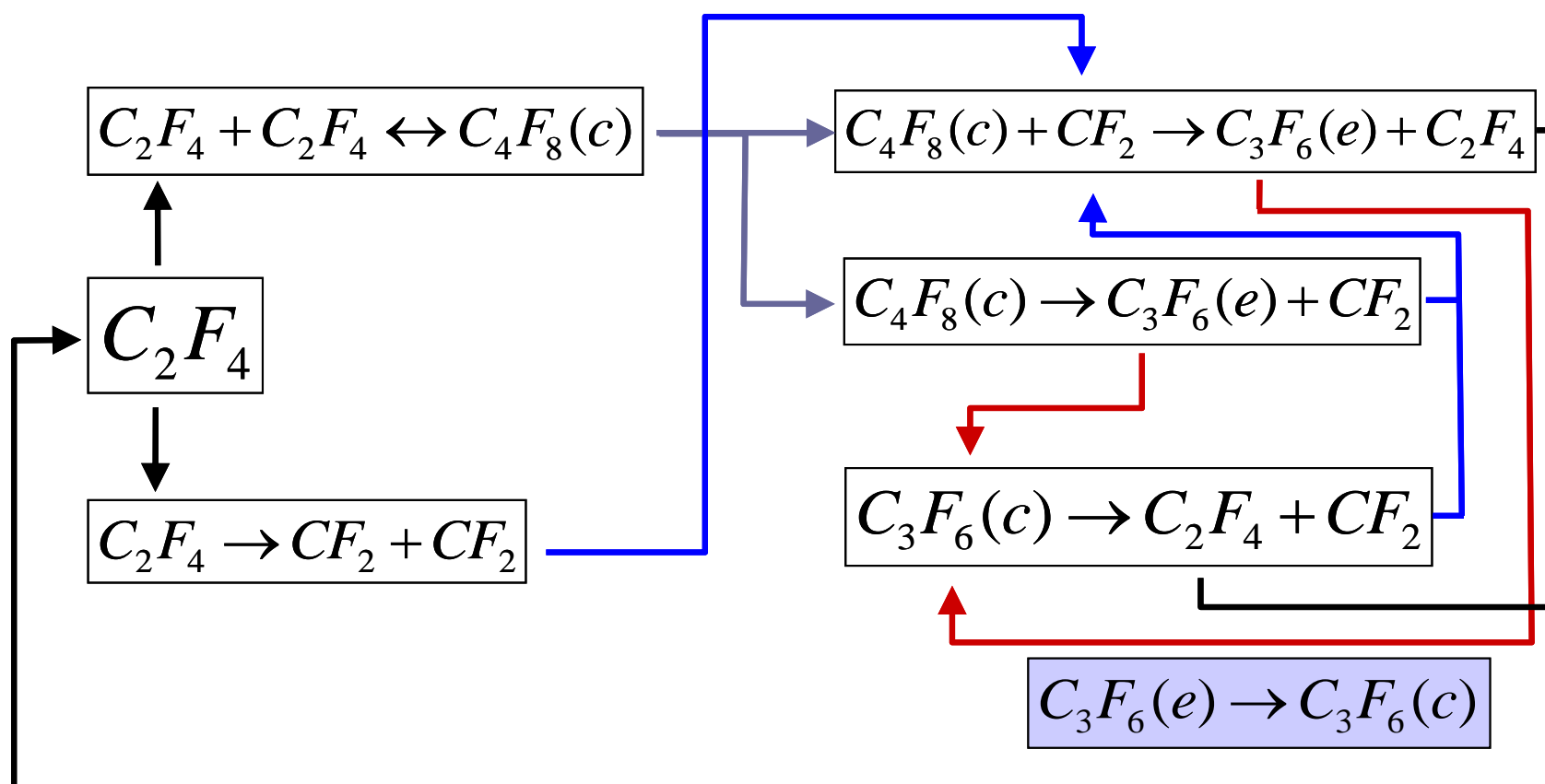
$$\Delta H_R = -103(\text{kJ}/\text{mol}_{\text{TFE}})$$

DECOMPOSITION



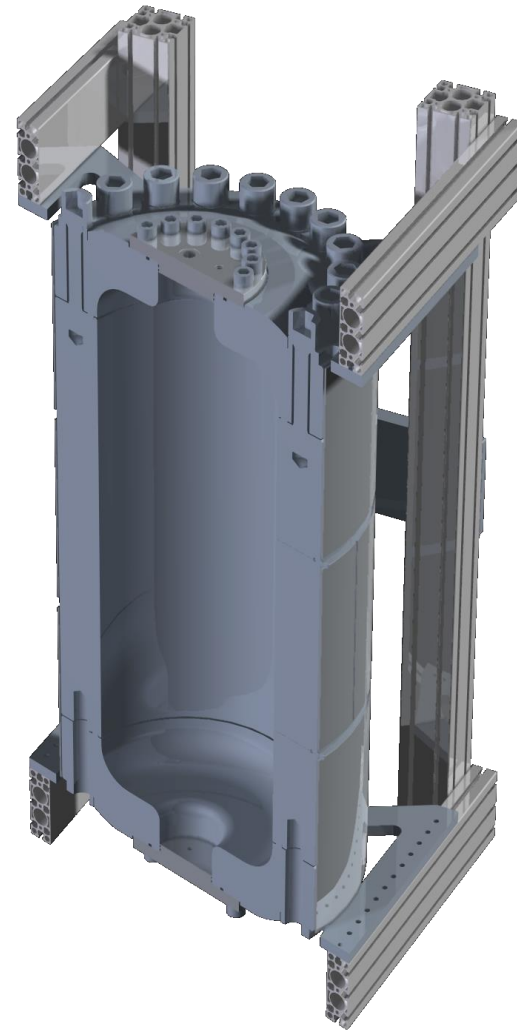
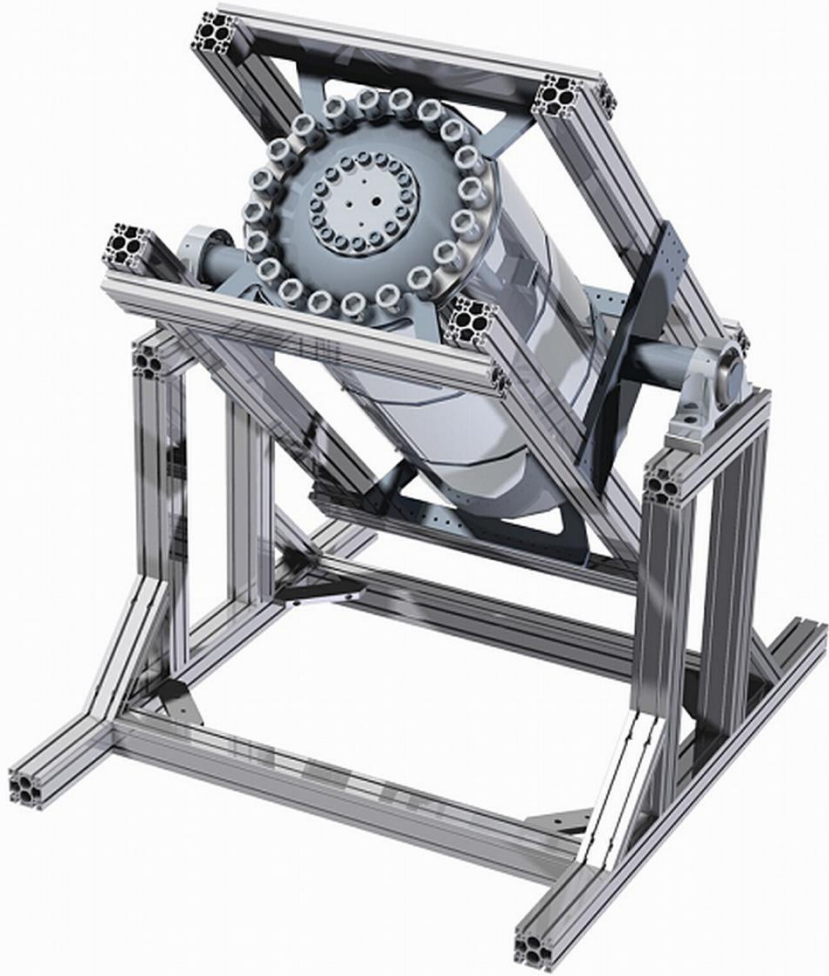
$$\Delta H_R = -257(\text{kJ}/\text{mol}_{\text{TFE}})$$

Extended reaction net*



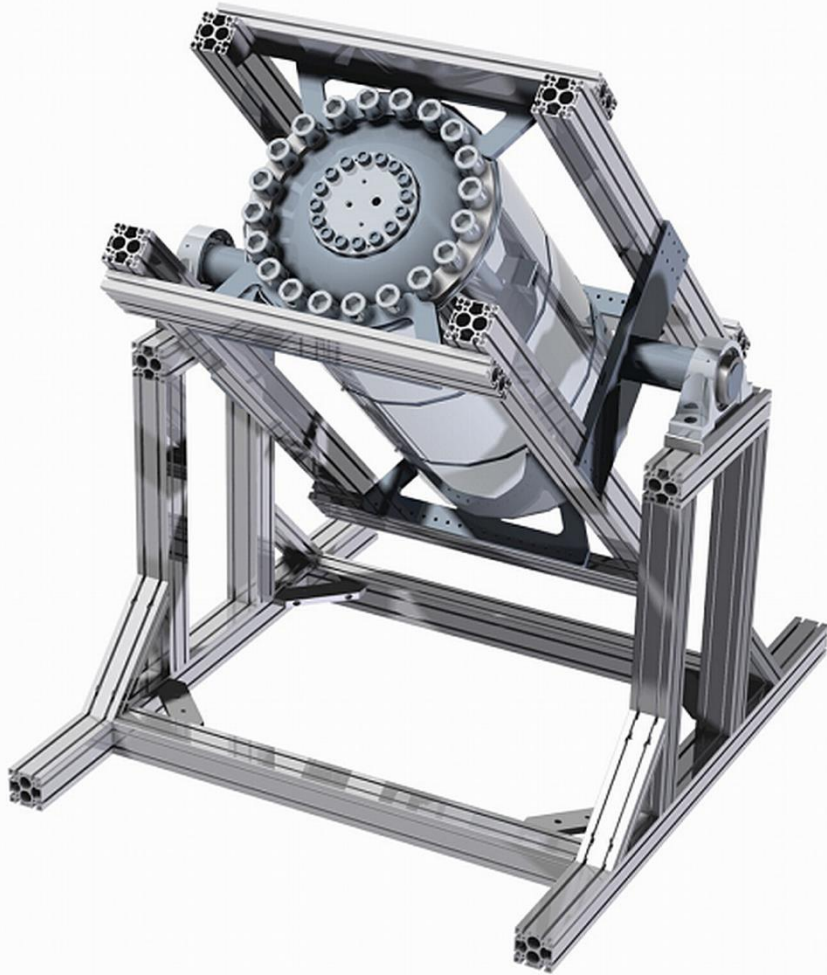
*Bauer, S.H., Javanovic, S., The Pyrolysis of Octafluorocyclobutane - Revisited, *International Journal of Chemical Kinetics*, 30, 171-177 (1998)

100-dm³-autoclave



Properties: • stainless steel • 1200 kg • 360° rotation • 345 bar(a) at 20 °C
Measurements: • temperature (up to 3 TC) • pressure

100-dm³-autoclave



Tests:

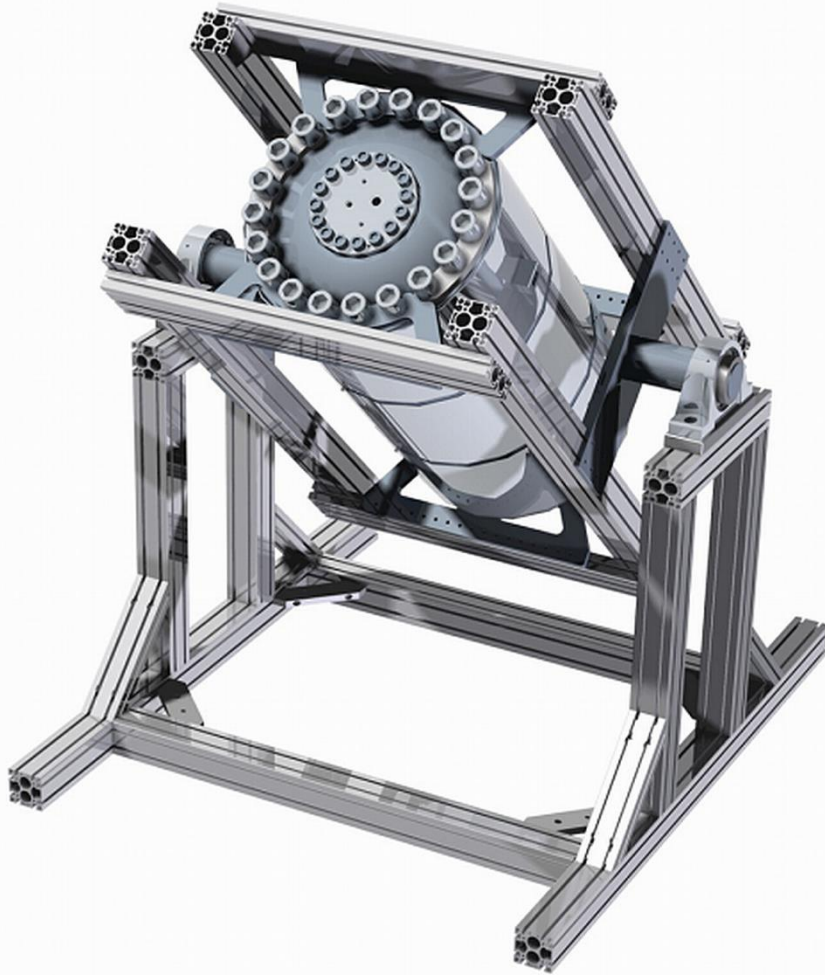
- $p_0 = 5, 10$ and 20 bar(a)
- $T_{\text{wall},0}$ is varied

=> lowest $T_{\text{wall},0}$ with an ignition

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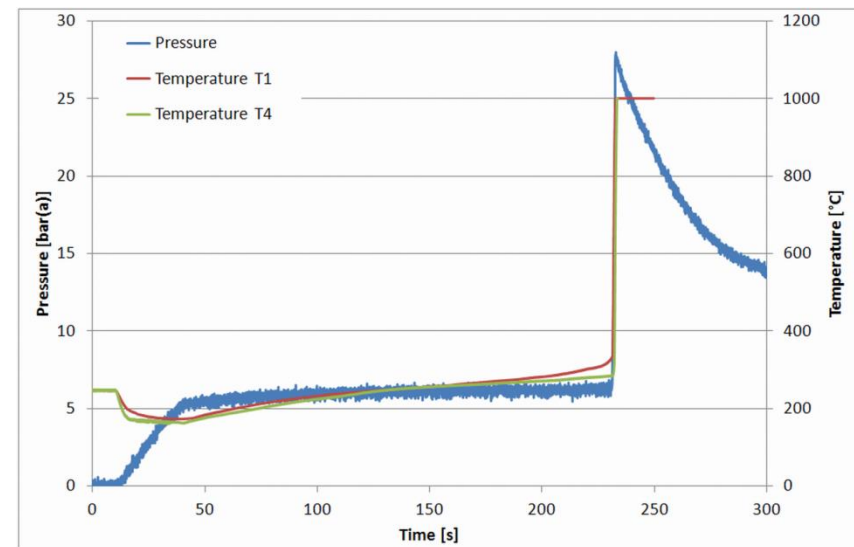
100-dm³-autoclave



Tests:

- $p_0 = 5, 10$ and 20 bar(a)
- $T_{\text{wall},0}$ is varied

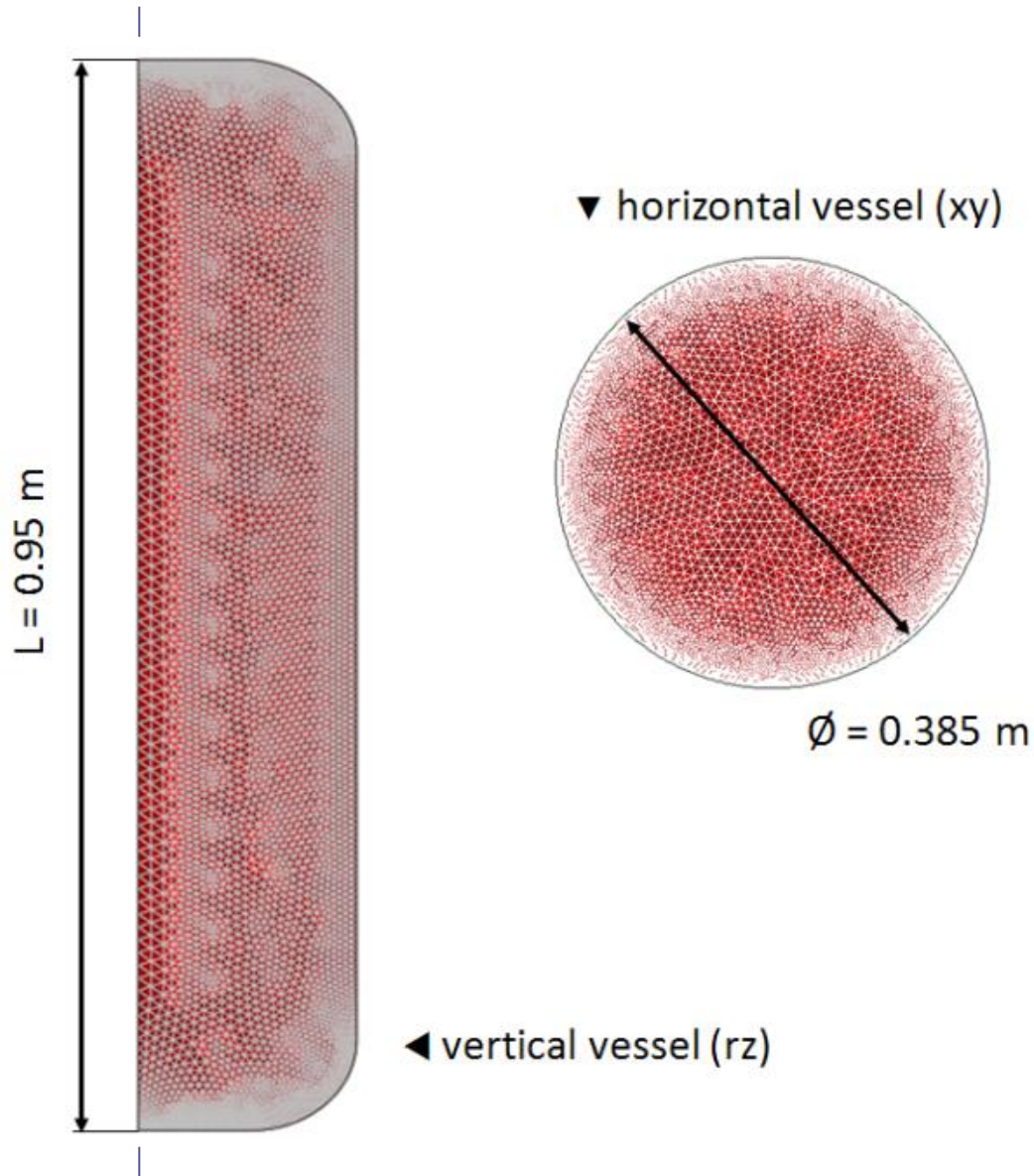
=> lowest $T_{\text{wall},0}$ with an ignition



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Measurements: • temperature (up to 3 TC) • pressure

Meshes (2D): only the TFE domain is computed



Quality > 0.85

Equations

$$\rho \frac{\partial \vec{u}}{\partial t} + \rho (\vec{u} \cdot \nabla) \vec{u} = -\nabla p + \eta \nabla^2 \vec{u} + \vec{F}$$

Momentum

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \vec{u}) = 0$$

Continuity

$$\rho c_P \frac{\partial T}{\partial t} = \nabla \cdot (\lambda \nabla T) - \rho c_P \vec{u} \cdot \nabla T + S_T$$

Heat transfer

$$\frac{\partial C_k}{\partial t} = \nabla \cdot (\mathbf{D}_k \nabla C_k) - \vec{u} \cdot \nabla C_k + S_{C_k}$$

Mass transfer

$$\rho = p / (R_s T)$$

Ideal gas law

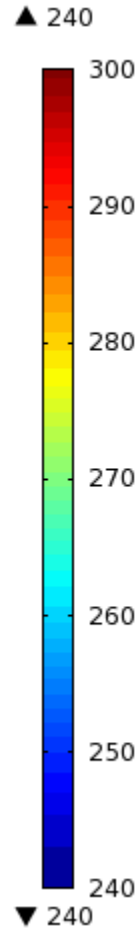
Chemical Engineering Module:

- non-isothermal flow mode (chns)
- convection and conduction mode (chcc)
- convection and diffusion mode (chcd)

Vertical Reactor

$p_0 = 11 \text{ bar(a)}$

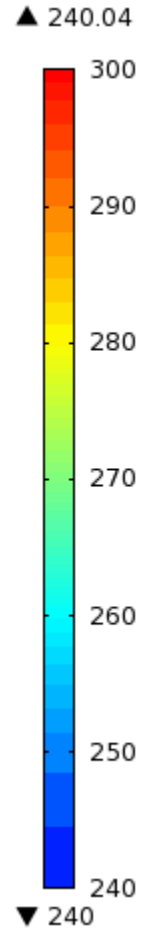
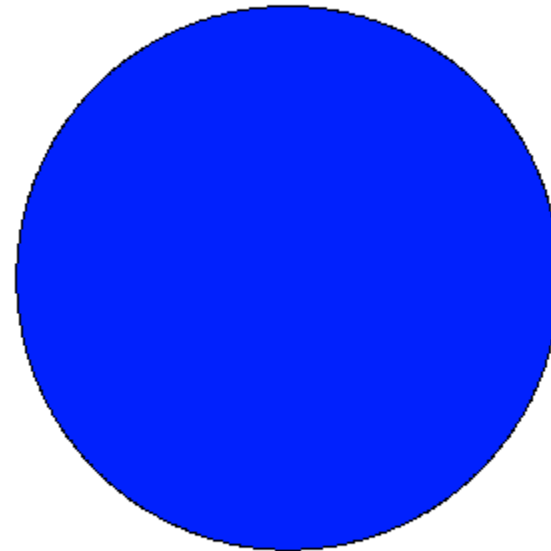
$T_0 = 240 \text{ °C}$



Horizontal Reactor

$p_0 = 11 \text{ bar(a)}$

$T_0 = 240 \text{ °C}$



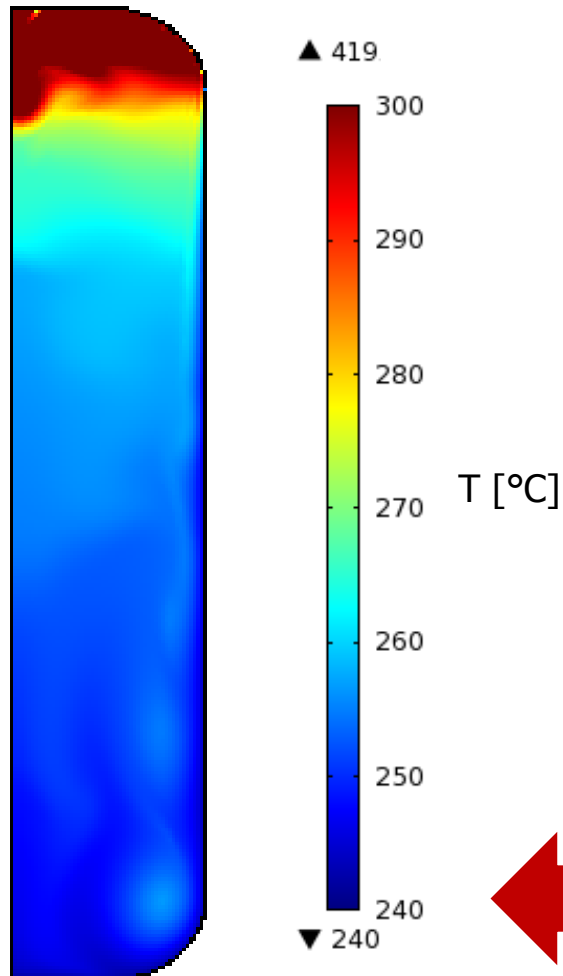
Time=0 Surface: Temperature (degC)

Vertical Reactor

$p_0 = 11 \text{ bar(a)}$

$T_0 = 240 \text{ °C}$

$t = 54 \text{ s}$

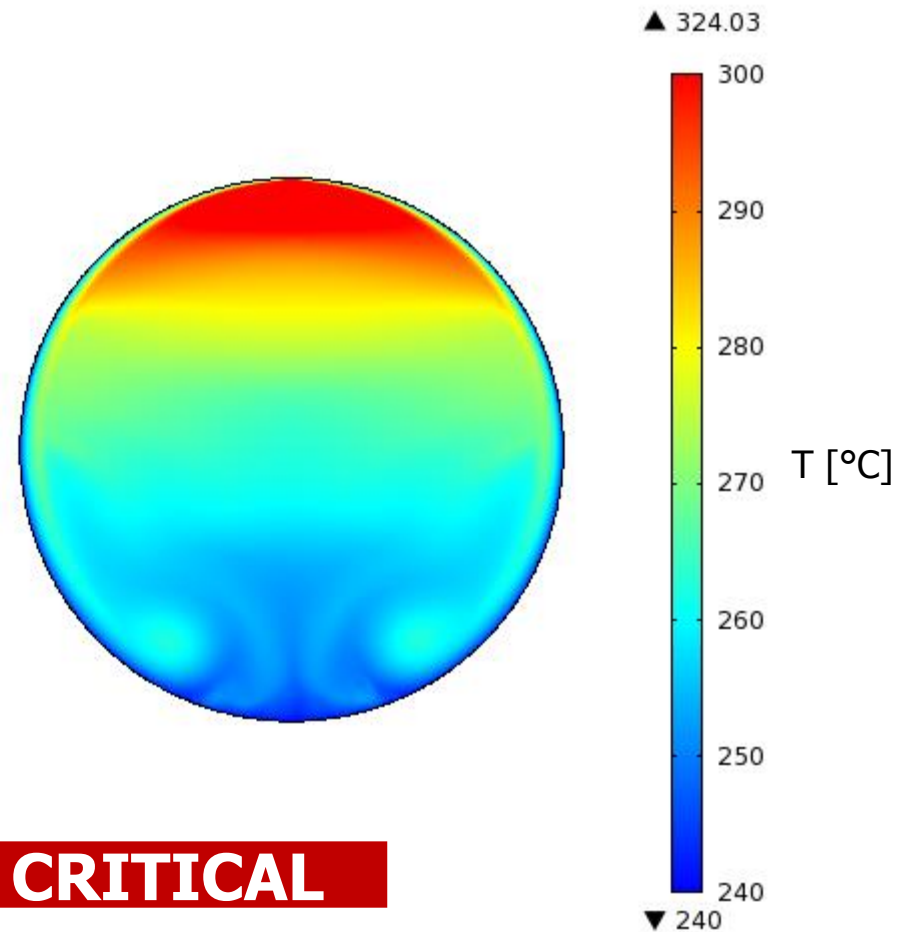


Horizontal Reactor

$p_0 = 11 \text{ bar(a)}$

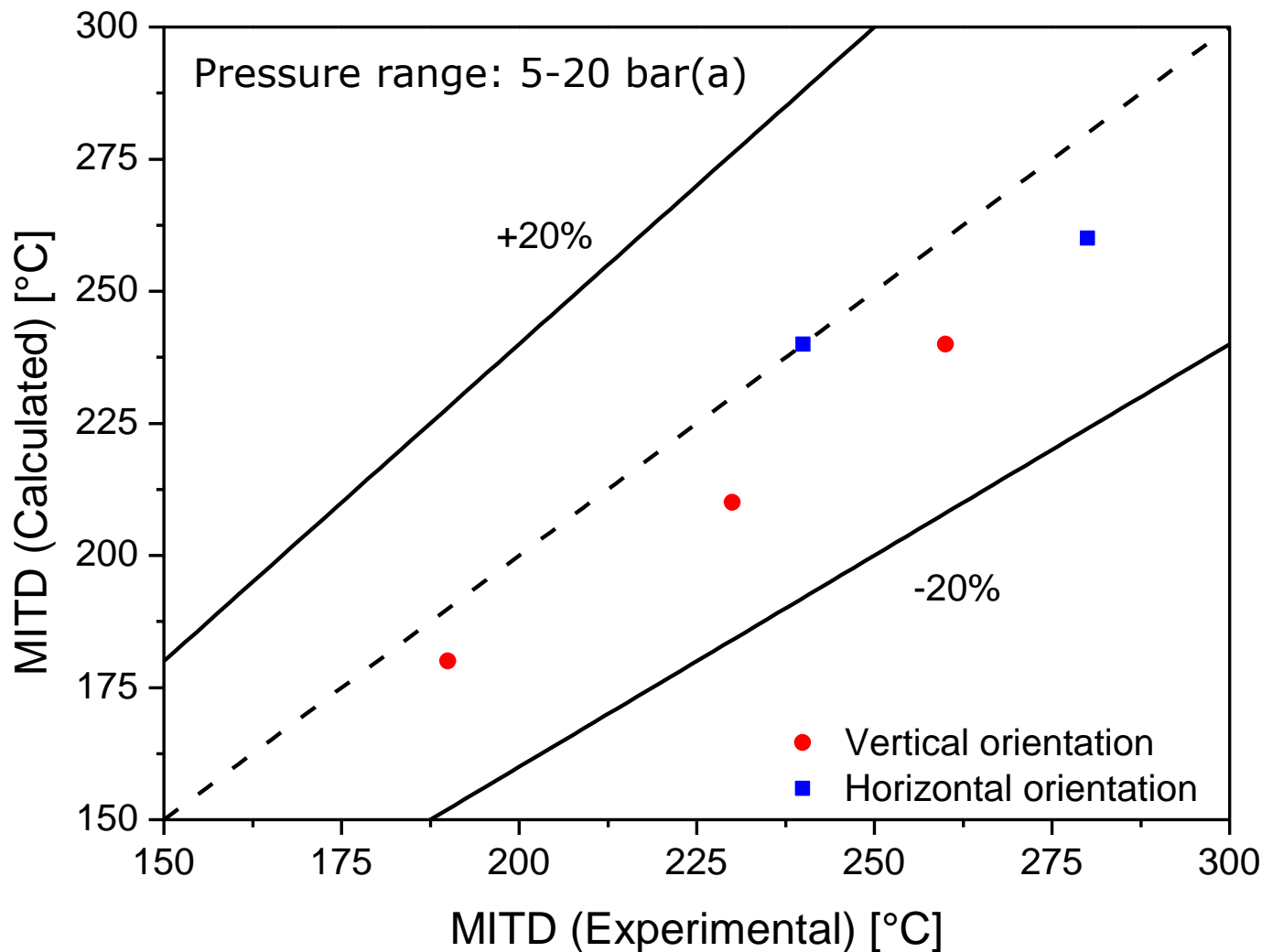
$T_0 = 240 \text{ °C}$

$t = 54 \text{ s}$



MORE CRITICAL

Prediction accuracy of TFE ignition temperatures (MITD)



- simulations of the self-ignition of TFE in a large scale vessel (100 dm³) were performed
- a good agreement with experimental data was observed
- in particular ignition temperatures of TFE were well predicted
- the model is considered validated for large geometries



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