

Comparison of different passive oil-water mixing schemes in a flow loop

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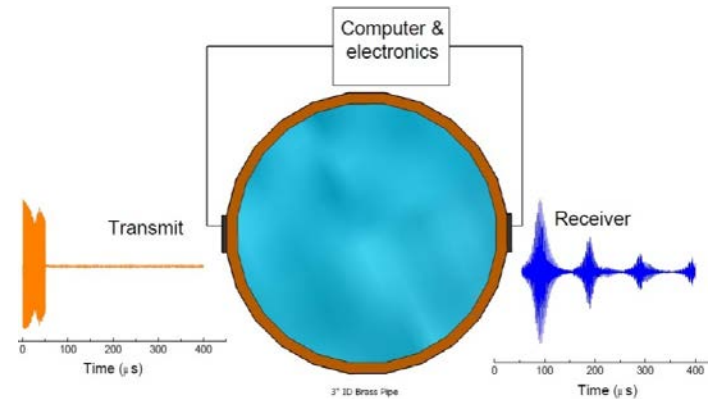
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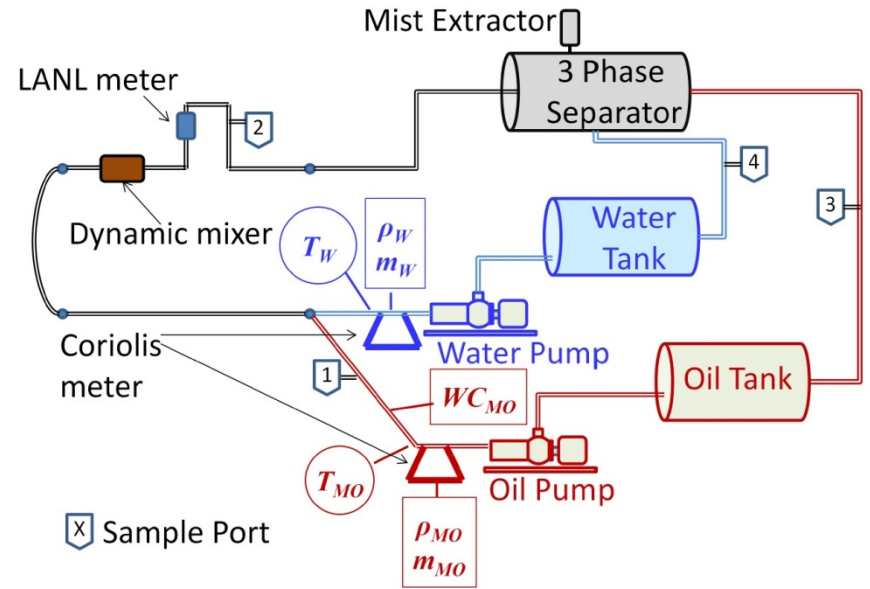
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Motivation

- Non-invasive composition measurement using ultrasound
- Transmitted acoustic signal is modified by fluid
- Process transmitted and received signals
 - Acoustic properties: sound speed, attenuation, density



Controlled flow tests at U-Tulsa

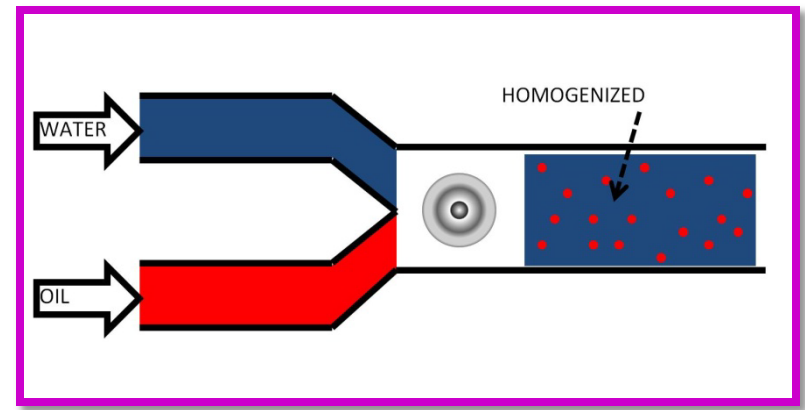
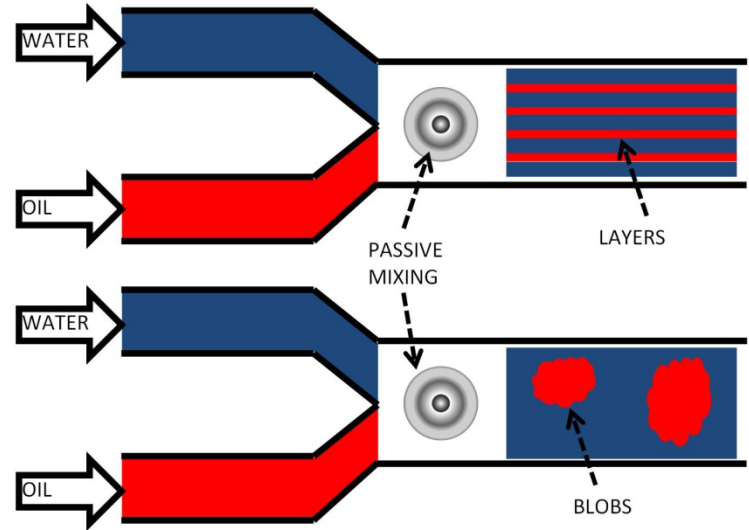


Chaudhuri et al., ASME J. Fluids Engg, 2014

- Proving tests for LANL measurement technique
- Ability to vary flow rate and composition
- Evaluate different scenarios from a test matrix

Lessons learnt

- Lack of proper mixing of two immiscible fluids – oil and water
 - Stratification due to separation of phases
 - Big blobs of oil
- Static mixer not completely effective under all test conditions
 - Needs dynamic mixing
 - What works best?

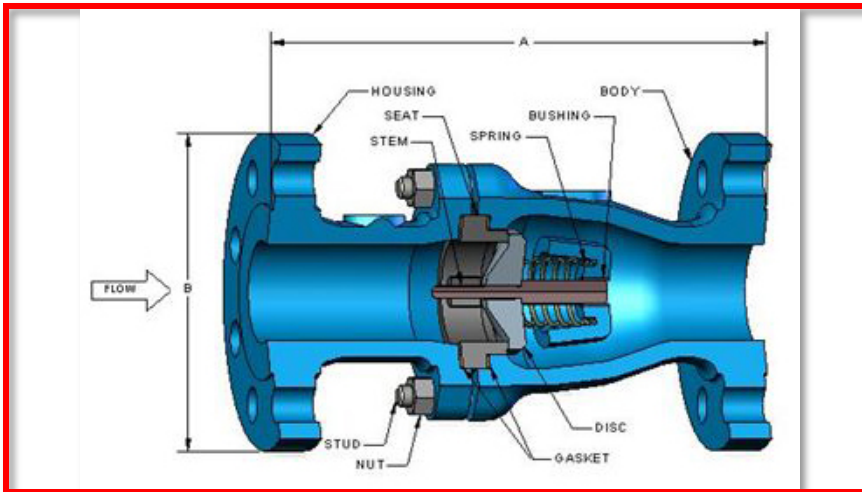


Passive mixing schemes

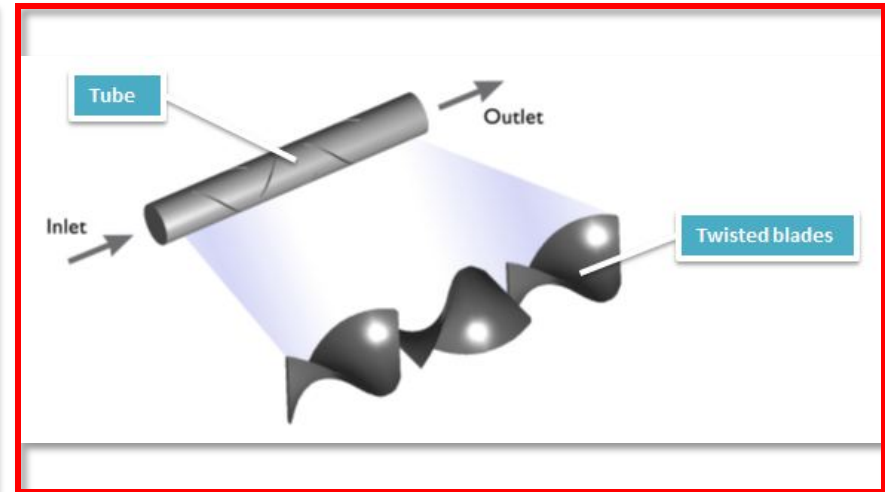
- Alter flow path by placing obstructions
- Easy to install and operate



BLIND-T



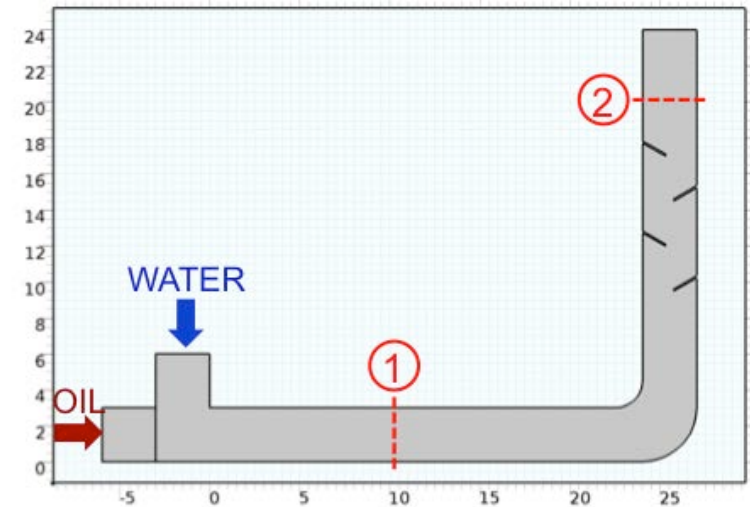
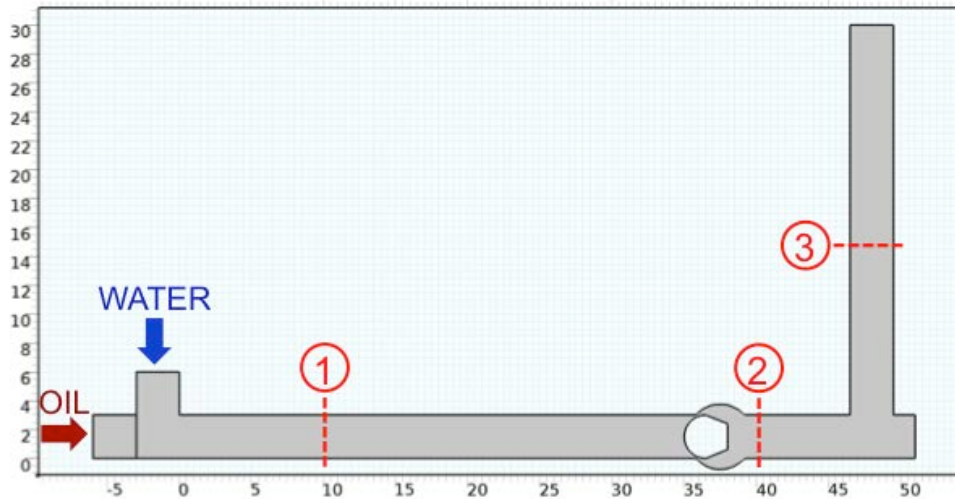
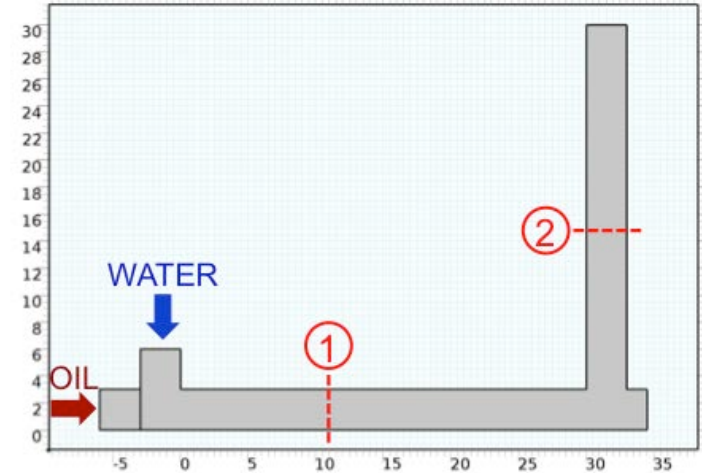
SPRING-LOADED CHECK VALVE



STATIC MIXER

Geometry, properties and inlet conditions

- 3" diameter pipe
 - Water: 1000 kg/m³, 1 cSt
 - Crude oil: 870 kg/m³, 100 cSt
- ϕ : volume fraction of oil
- U_{in} : total liquid velocity
 - Oil inlet velocity = ϕU_{in}
 - Water inlet velocity = $(1-\phi) U_{in}$



Physics

- 2-D Multiphase Flow physics – COMSOL CFD
- Two-Phase Laminar Flow Level Set (*tpf*)
 - Low Reynolds numbers
- Transient solver
 - Capture evolution of flow

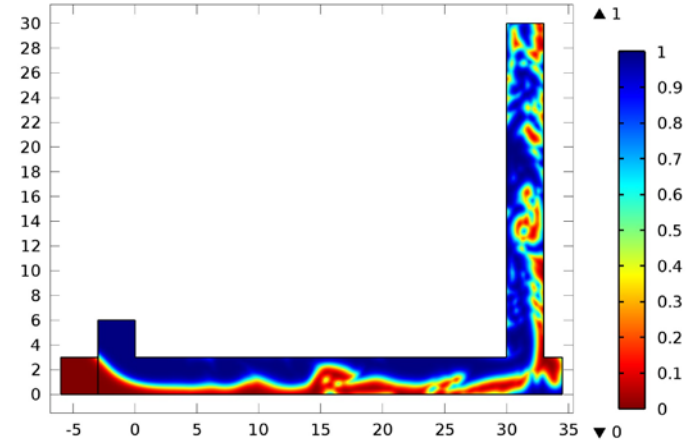
$$\rho \frac{\partial \mathbf{u}}{\partial t} - \nabla \cdot \eta \left(\nabla \mathbf{u} + (\nabla \mathbf{u})^T \right) + \rho (\mathbf{u} \cdot \nabla) \mathbf{u} + \nabla p = 0$$

$$\nabla \cdot \mathbf{u} = 0$$

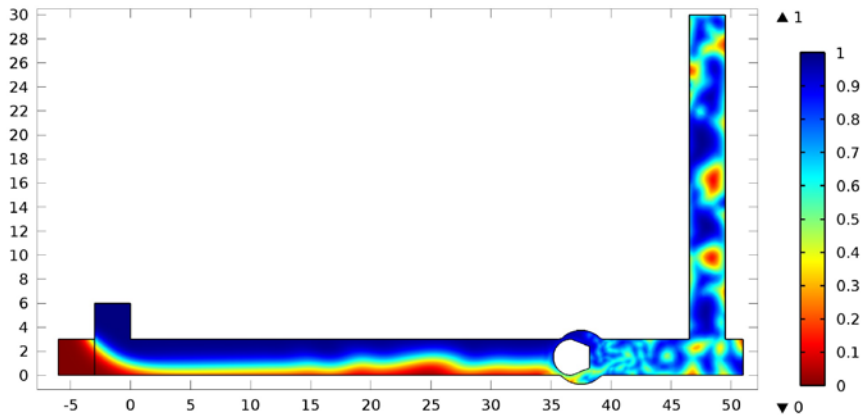
Results

- Distribution of oil and water phases
 - Time evolution
- Lack of homogeneity

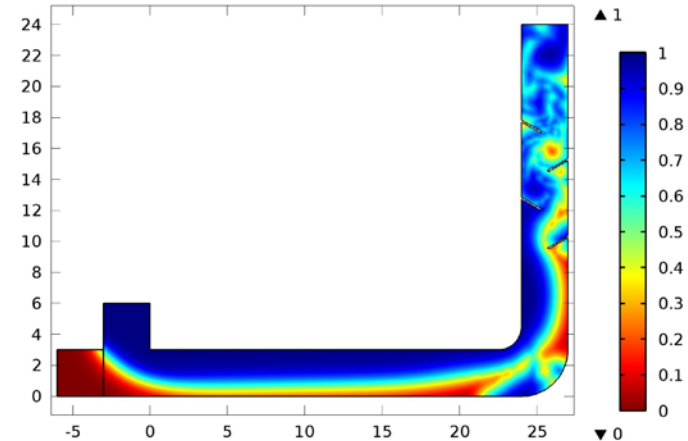
Uin=1, oilvolfrac=0.3 Time=4 s Surface: Volume fraction of fluid 1 (1)



valveposition=0.8, Uin=1, oilvolfrac=0.3 Time=3.6 s Surface: Volume fraction of fluid 1 (1)



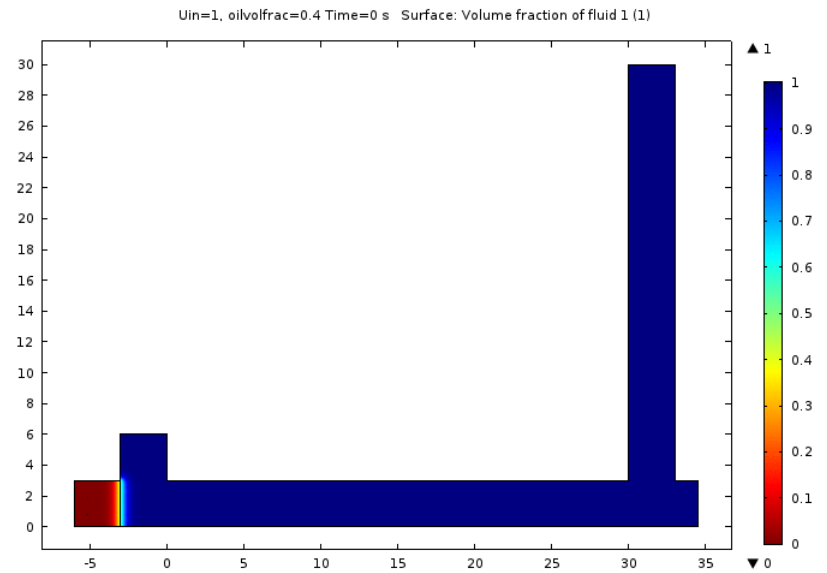
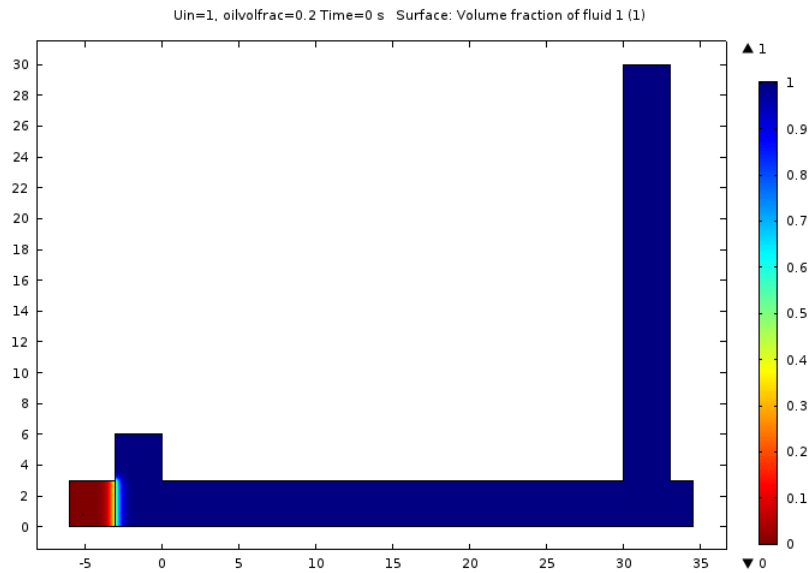
Uin=1, oilvolfrac=0.3 Time=3 s Surface: Volume fraction of fluid 1 (1)



Transient flow – Blind T

$$\phi = 0.2$$

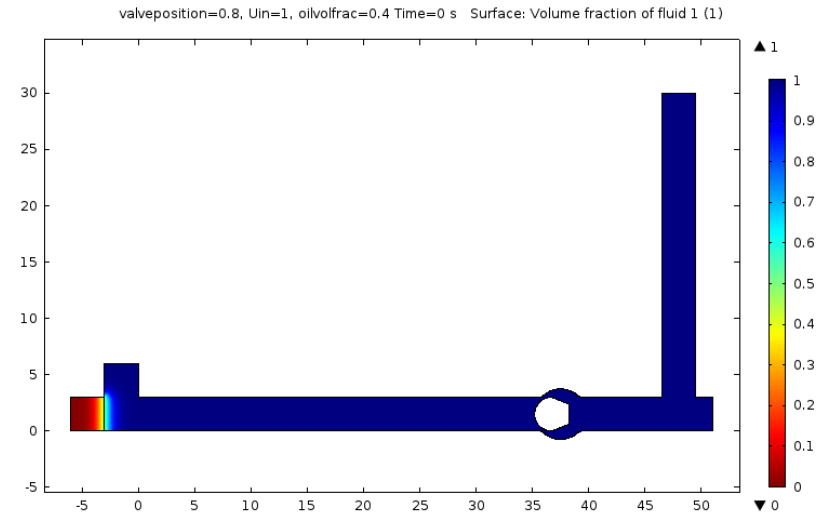
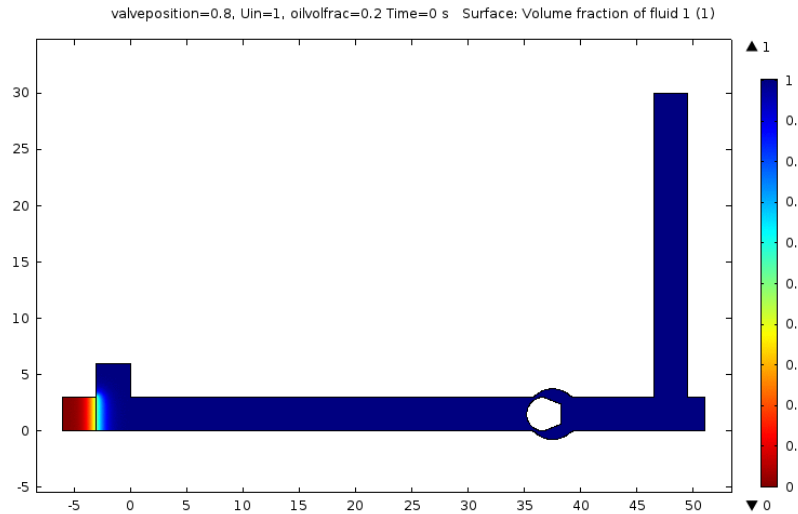
$$\phi = 0.4$$



Transient flow – Check valve

$$\phi = 0.2$$

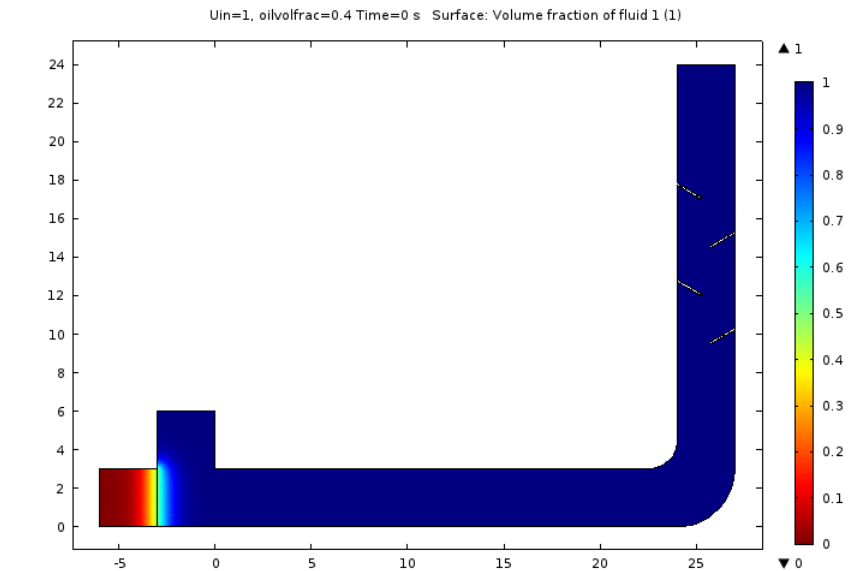
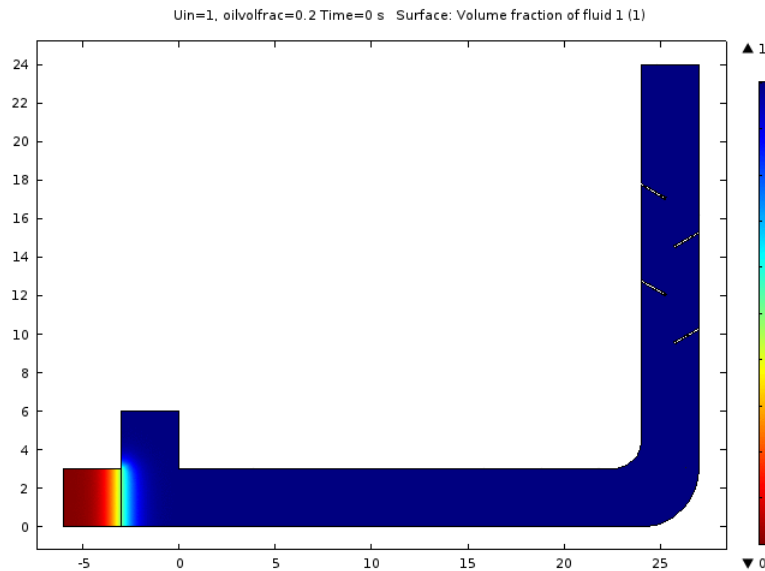
$$\phi = 0.4$$



Transient flow – Static mixer

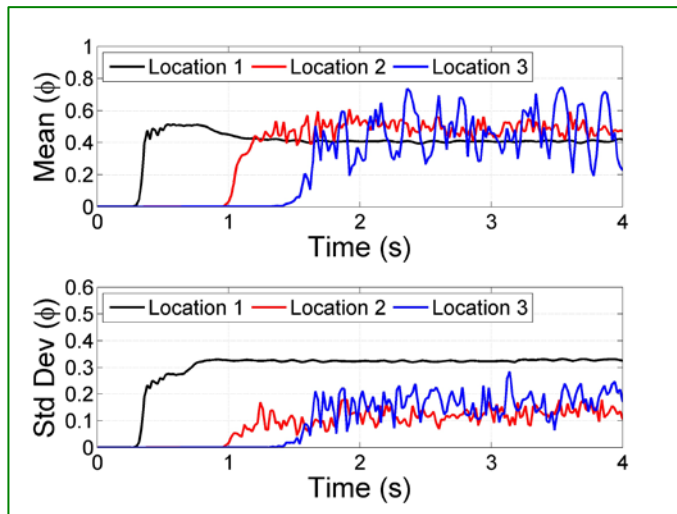
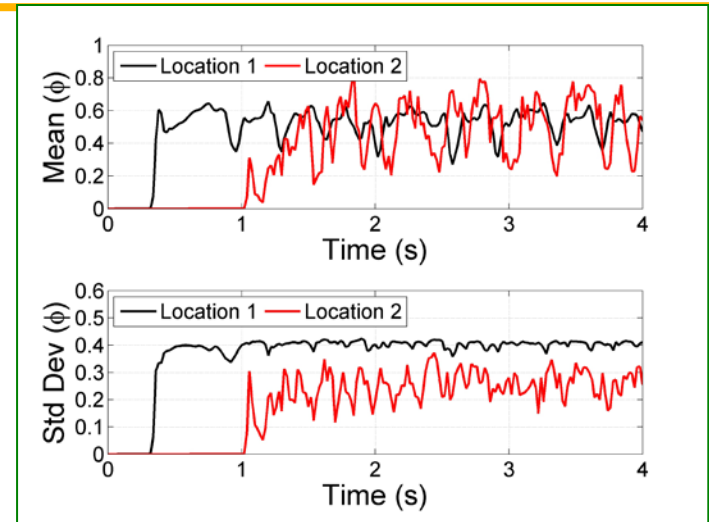
$$\phi = 0.2$$

$$\phi = 0.4$$

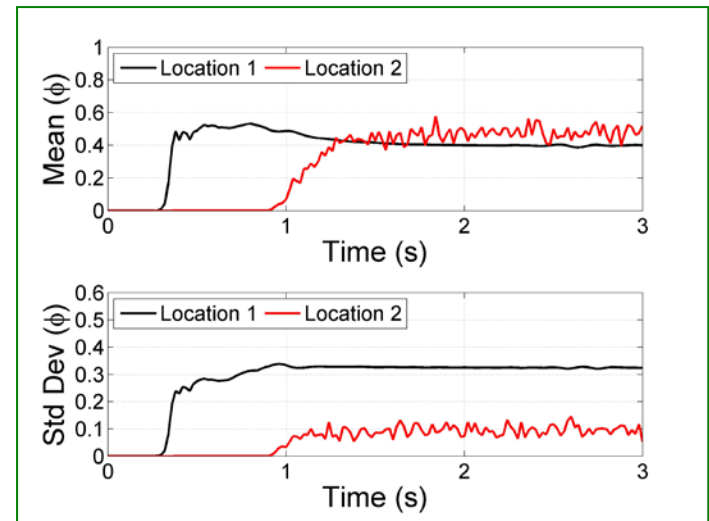


Compare 3 devices: $\phi_{set} = 0.5$, $U_{in} = 1 \text{ m/s}$ BLIND-T

- Mean volume fraction nearly same
 - Mass continuity
- Variation in ϕ is lower downstream of device
 - Homogeneity due to mixing

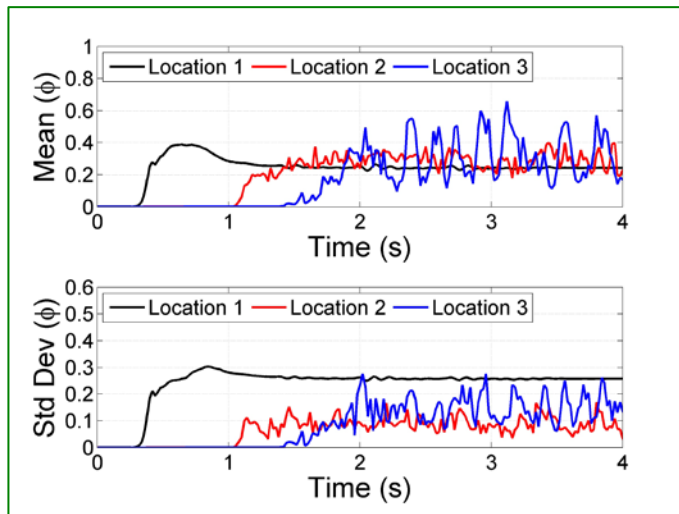
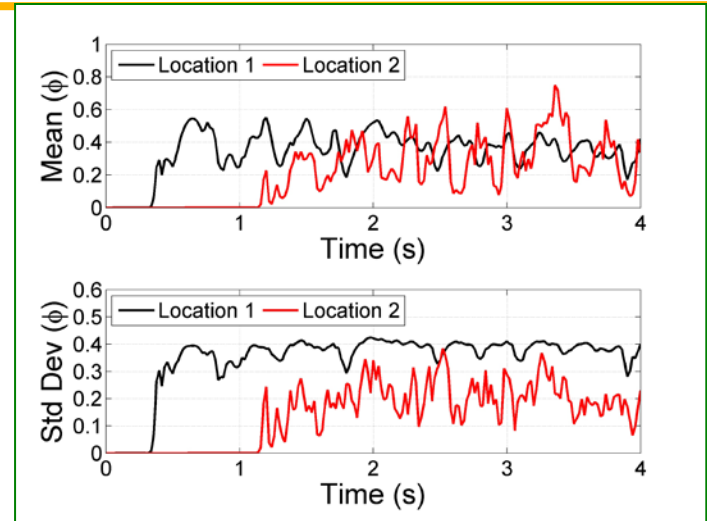


SPRING-LOADED CHECK VALVE

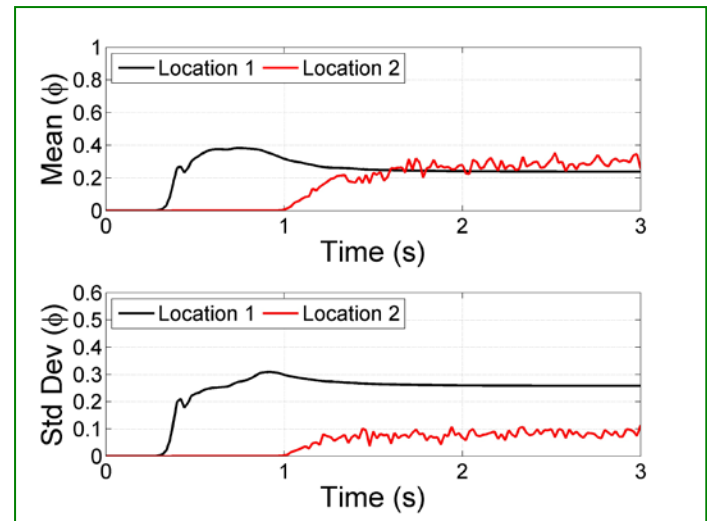


STATIC MIXER

Compare 3 devices: $\phi_{set} = 0.3, U_{in} = 1 \text{ m/s}$ BLIND-T

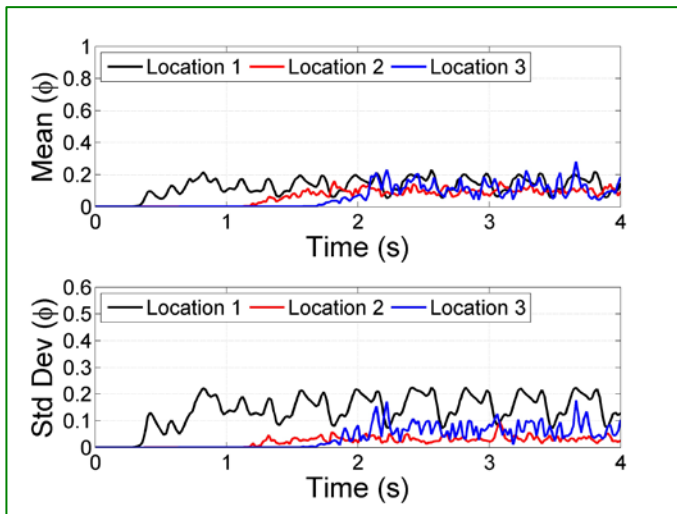
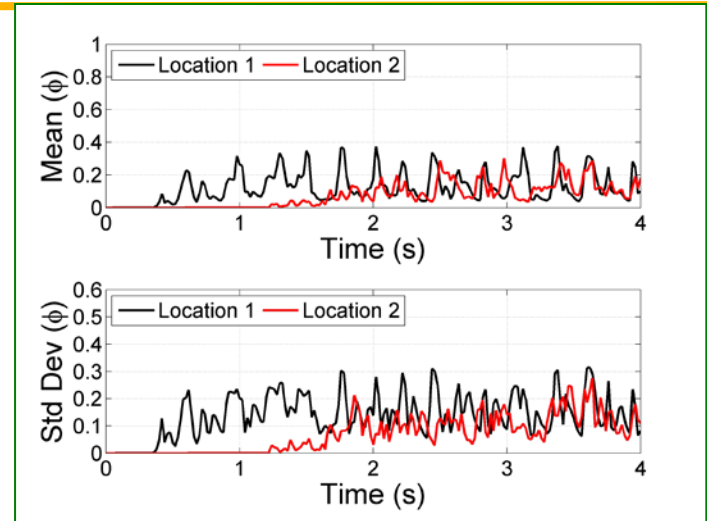


SPRING-LOADED CHECK VALVE

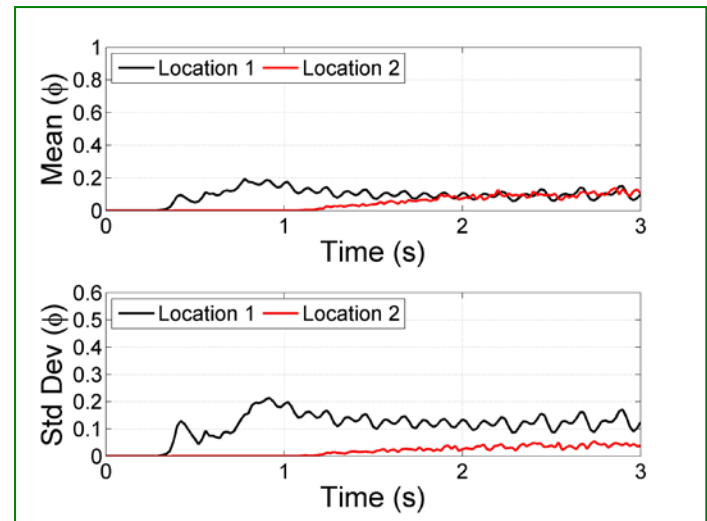


STATIC MIXER

Compare 3 devices: $\phi_{set} = 0.1, U_{in} = 1 \text{ m/s}$ BLIND-T



SPRING-LOADED CHECK VALVE



STATIC MIXER

Summary

- Injecting two immiscible fluids into a single pipe does not result in a homogeneous mixture and there are large variations in local properties
- Introduction of passive mixing schemes improves homogeneity of the mixture but their effectiveness depends on physical configuration