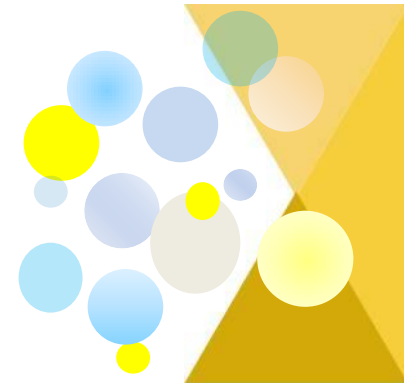


Investigating Magnetic and Electric Fields Couplings for 3D models in Harmonic and Transient States

O. MALOBERTI
O. MANSOURI
(ESIEE Amiens)



Context and Goal

- **Context:**

Pulsed magnetic technologies

Medium frequencies – pulsed magnetic fields

Eddy currents, skin effect and Lorentz force

- **Goal:**

Investigate a 3D harmonic and transient formulation coupling magnetic and electric fields formulations in COMSOL

Summary

- 1. Introduction: 2 or 3 test cases
- 2. Governing and resulting equations
- 3. Modelling of test cases and results
 - 3.1. Presentation of Test Case 1 – the wire
 - 3.2. Presentation of Test Case 2 – the wire in air
 - 3.3. Presentation of Test Case 3 – the coil
- 4. Conclusion and Forthcomings

1. Introduction

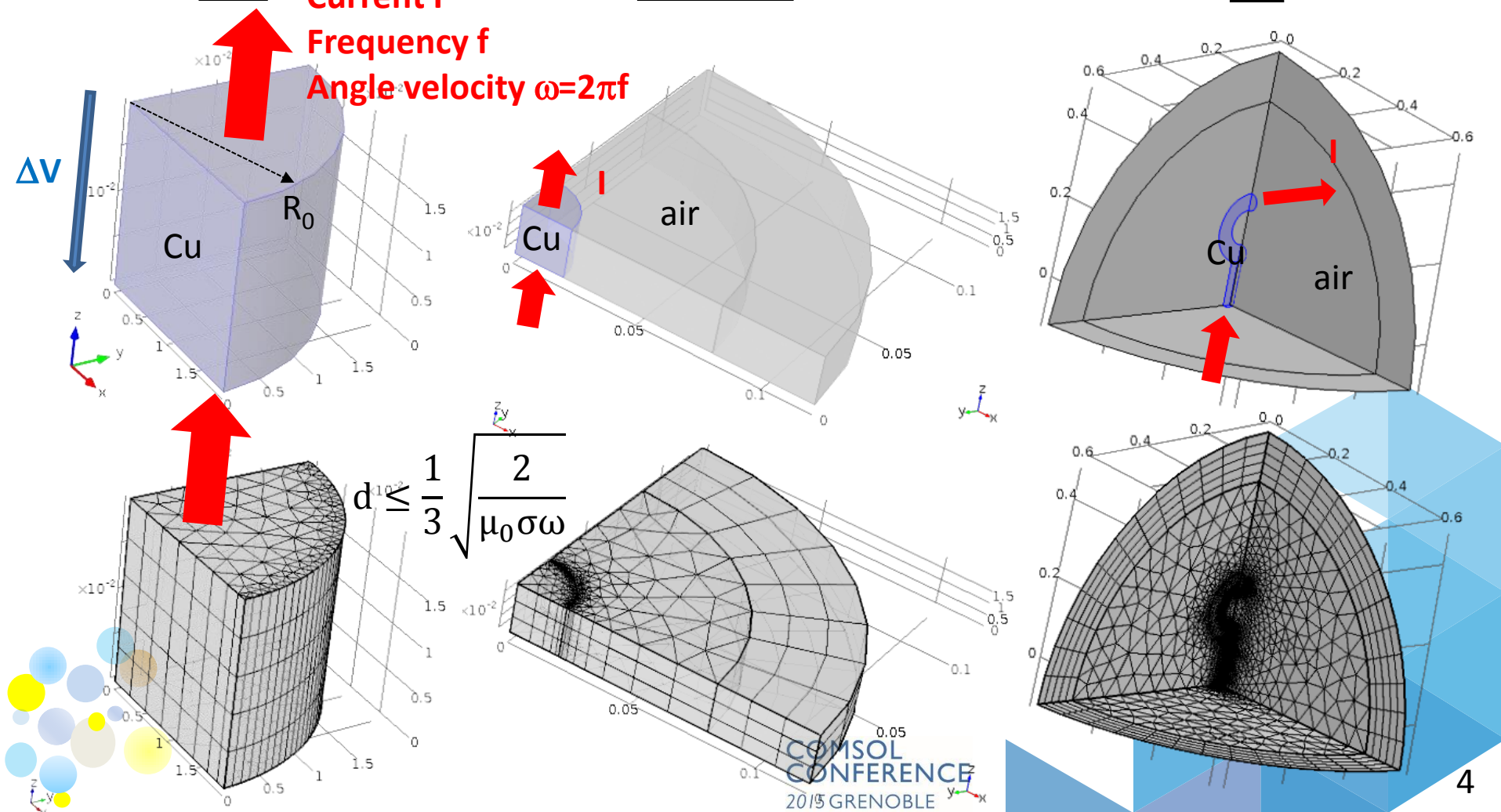
Conducting material: Copper (Conductivity $\sigma \cong 6e^7 \text{ S.m}^{-1}$, permeability $\mu = \nu^{-1} = \mu_0 = \nu_0^{-1} = 4\pi \cdot e^{-7} \text{ H.m}^{-1}$, permittivity $\epsilon = \epsilon_0 = 8.85 \cdot e^{-12} \text{ F.m}^{-1}$)

wire

Current I
Frequency f
Angle-velocity $\omega = 2\pi f$

wire in air

coil



2. Governing Equations

- Magnetic Field – Magnetic Vector Potential **A**:

$$\left\{ \begin{array}{l} \nabla \times \mathbf{H} = \mathbf{j} \text{ and } \mathbf{H} = \nu \mathbf{B} = \nu_0 \mathbf{B} \\ \text{with } \mathbf{B} = \nabla \times \mathbf{A} \end{array} \right\}$$

- Electric Field – Electric Scalar Potential V :

$$\left\{ \begin{array}{l} \nabla \cdot \mathbf{j} = 0 \text{ and } \mathbf{j} = \sigma \mathbf{E} \\ \text{with } \mathbf{E} = -\nabla V \end{array} \right\}$$

- Coupling potentials **A** and V :

$$\left\{ \begin{array}{l} \nabla \times (\nu \nabla \times \mathbf{A}) + \sigma \partial_t \mathbf{A} = -\sigma \nabla V \\ \nabla \cdot \mathbf{A} = 0 \end{array} \right\}$$

with $\mathbf{B} = \nabla \times \mathbf{A}$ and $\mathbf{E} = -\nabla V - \partial_t \mathbf{A}$

2. Resulting Equations

- Power losses and equivalent resistance

$$P_j = \iiint_{\text{space}} \frac{j^2}{2\sigma} d^3x \quad \text{and} \quad R = \frac{2P_j}{I^2} \quad \text{with} \quad I = \iint_{\pi R_0^2} \mathbf{j} \cdot d^2\mathbf{x}$$

- Magnetic energy and equivalent inductance

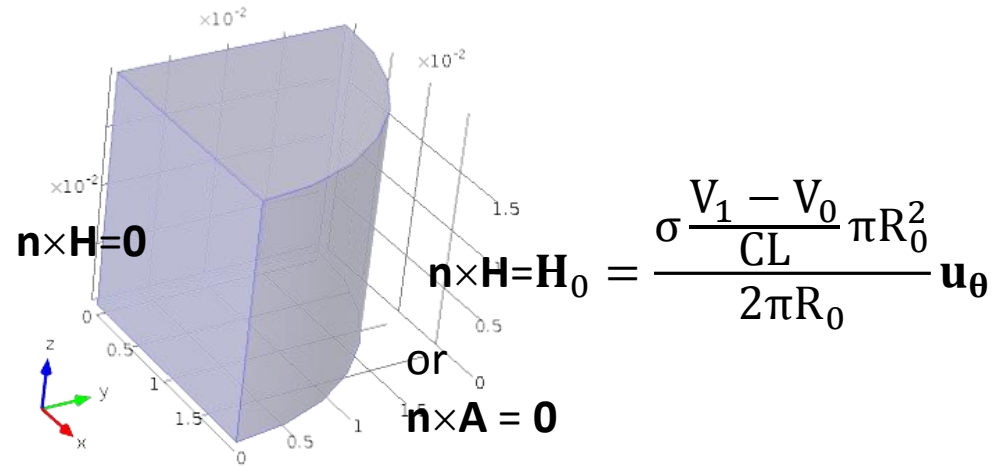
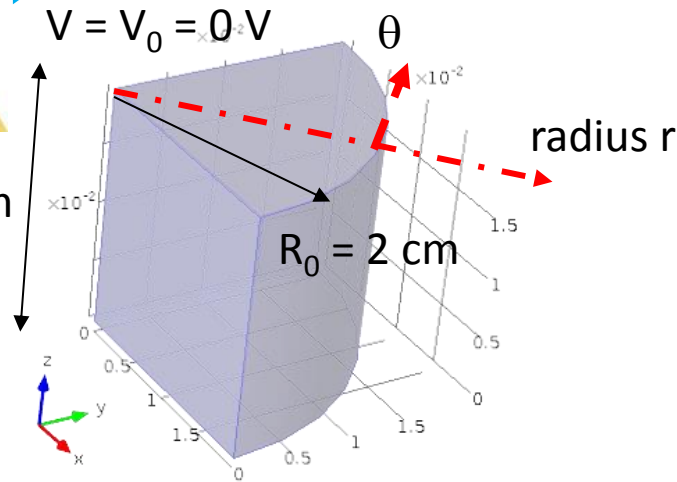
$$W_m = \iiint_{\text{space}} \frac{B^2}{2\mu} d^3x \quad \text{and} \quad L = \frac{2W_m}{I^2}$$

- Electric energy and equivalent capacity

$$W_e = \iiint_{\text{space}} \frac{D^2}{2\varepsilon} d^3x \quad \text{and} \quad C = \frac{2W_e}{(\Delta V)^2}$$

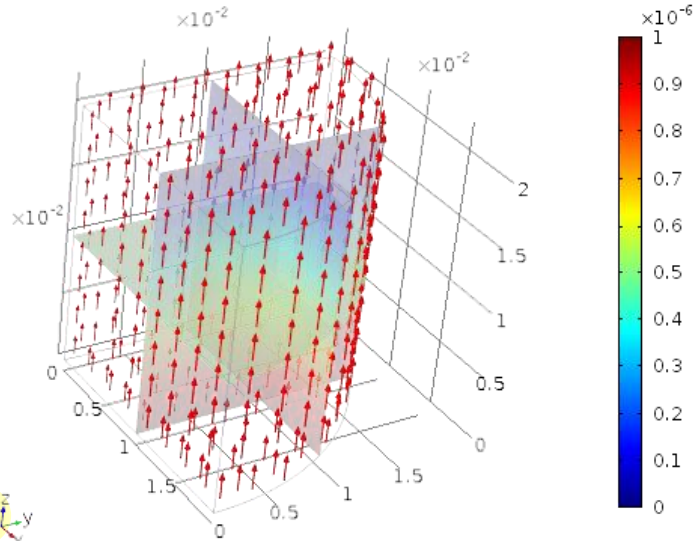
3. Modelling of test cases

3.1. Test case 1 - *the wire*



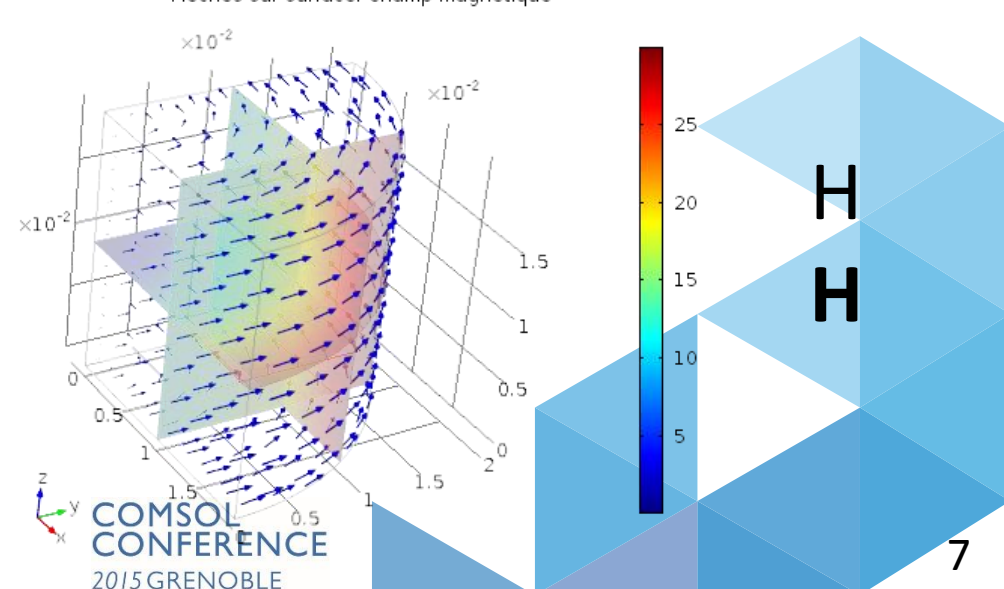
$V = V_1 = 1 \mu\text{V} = 1 \text{ e}^{-6} \text{ V}$

freq0(5)=50 freq(1)=50 Multicoups: Potentiel électrique (V)
Flèches sur surface: Densité de courant



V
j

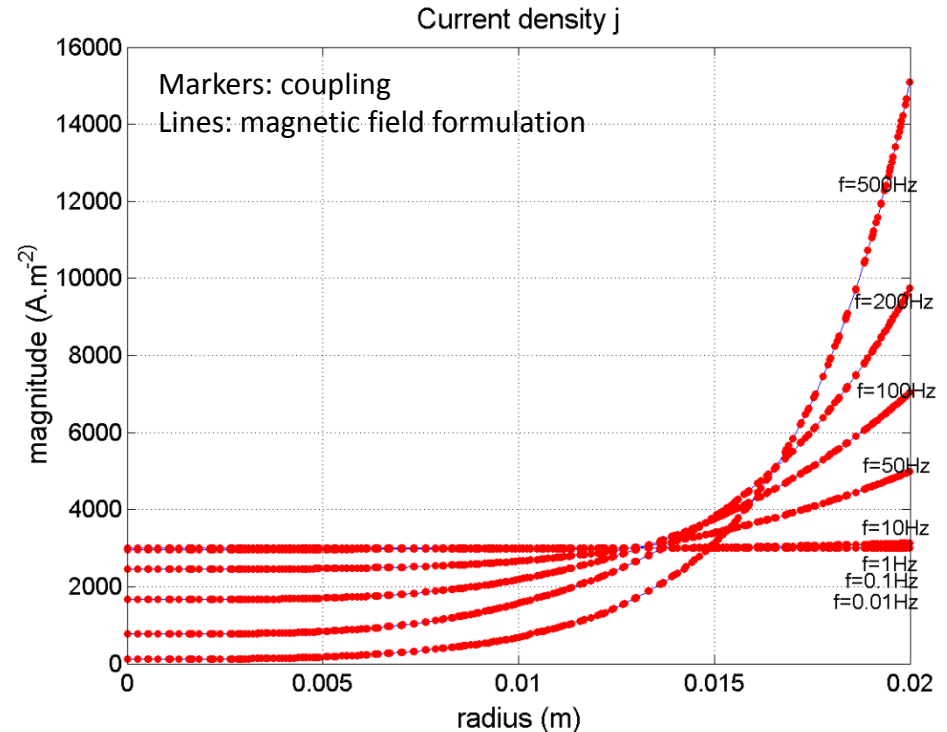
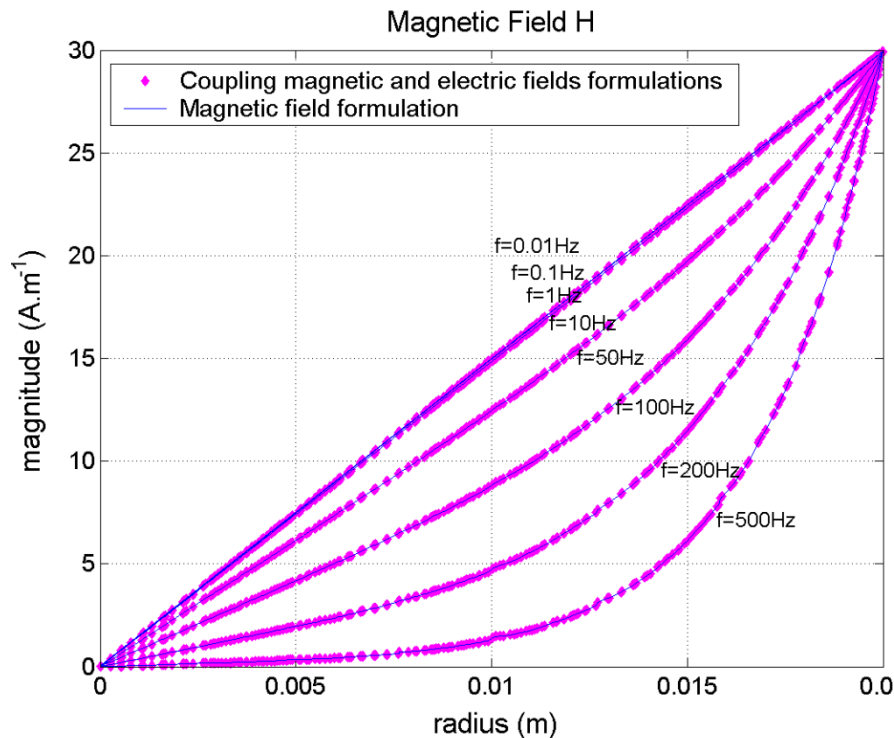
freq0(5)=50 freq(1)=50 Multicoups: Champ magnétique, norme (A/m)
Flèches sur surface: Champ magnétique



3. Modelling of test cases

3.1. Test case 1 - *the wire*

- H and j distribution with field constraint

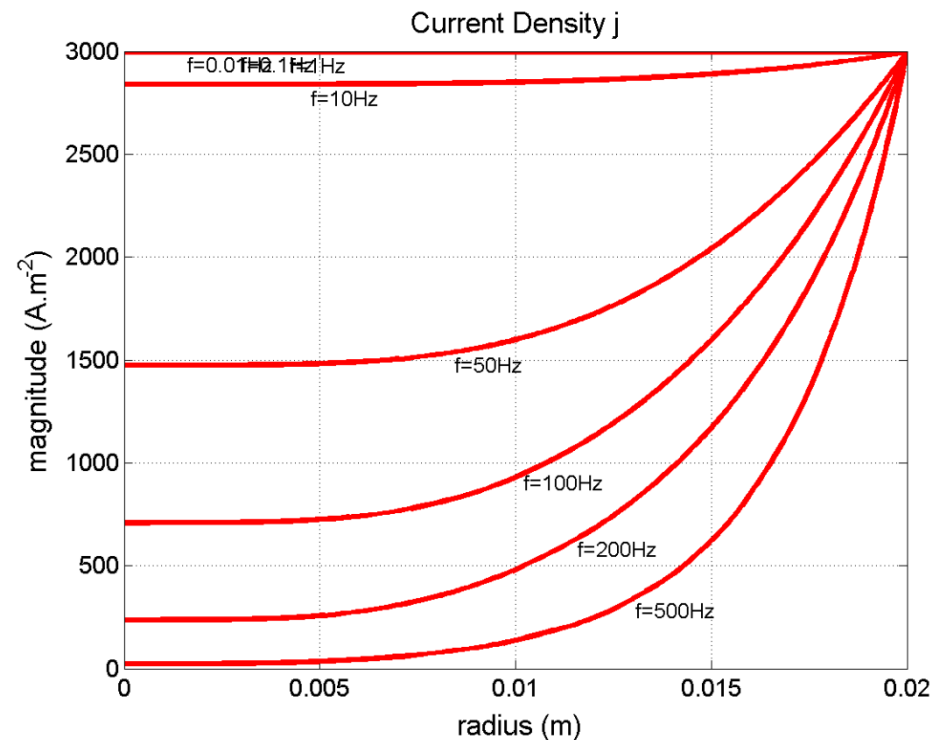
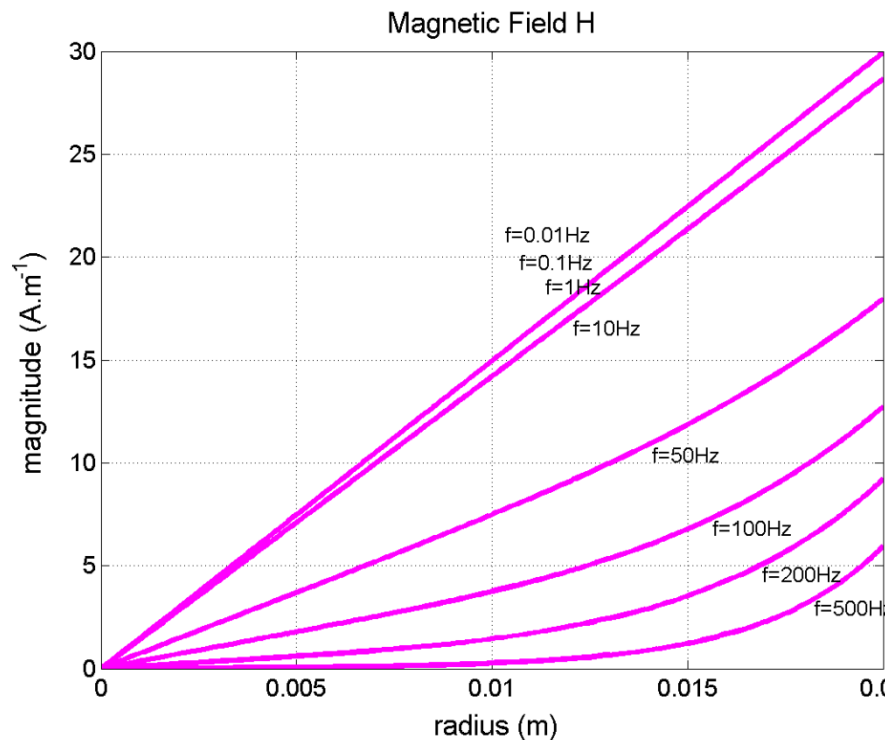


- Eddy currents and skin effect correctly described
- Agreement between the two methods and formulations

3. Modelling of test cases

3.1. Test case 1 - *the wire*

- H and j distribution without field constraint

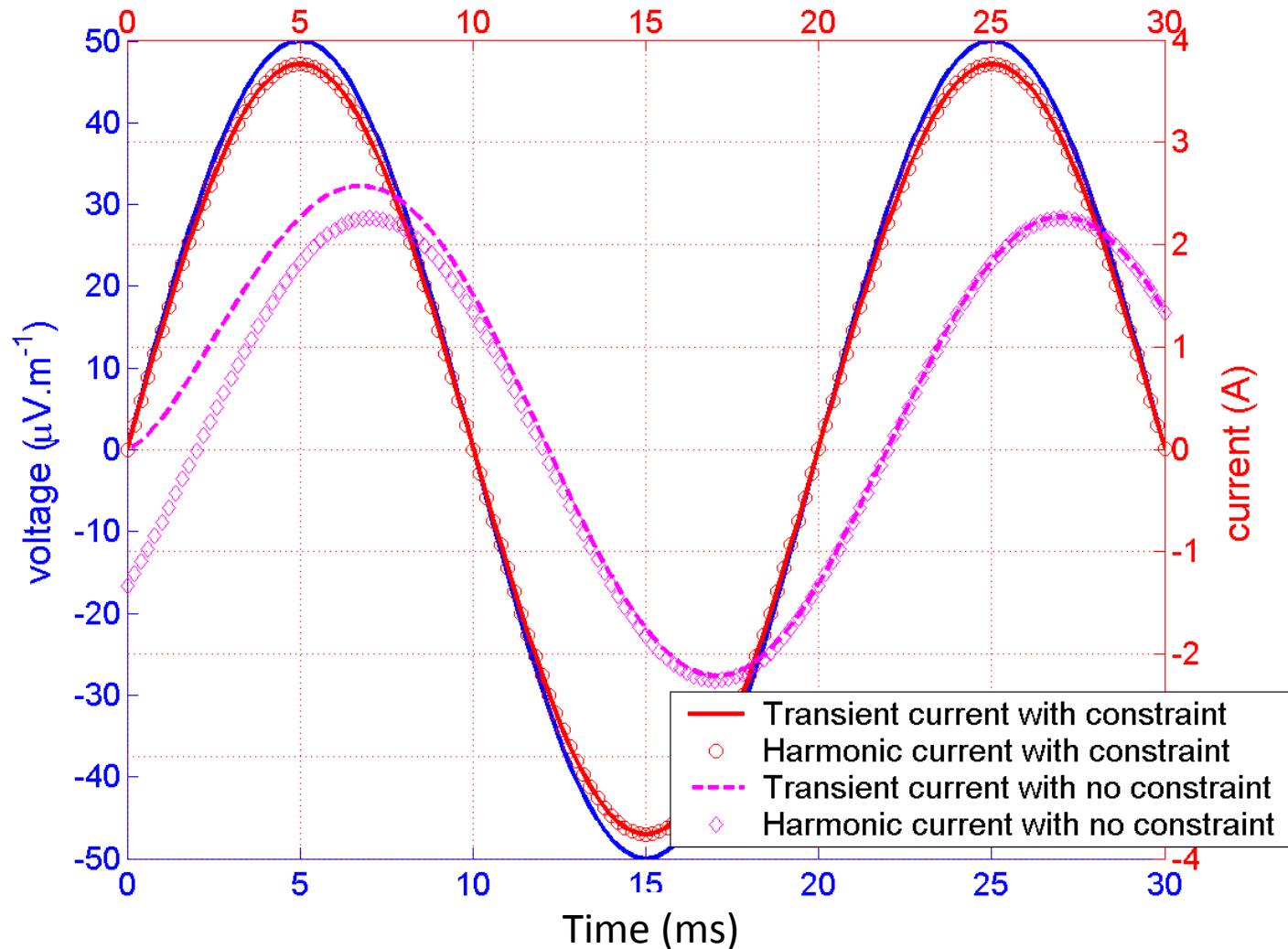


- Eddy currents and skin effect correctly described
- Electric field and total current density damping

3. Modelling of test cases

3.1. Test case 1 - *the wire*

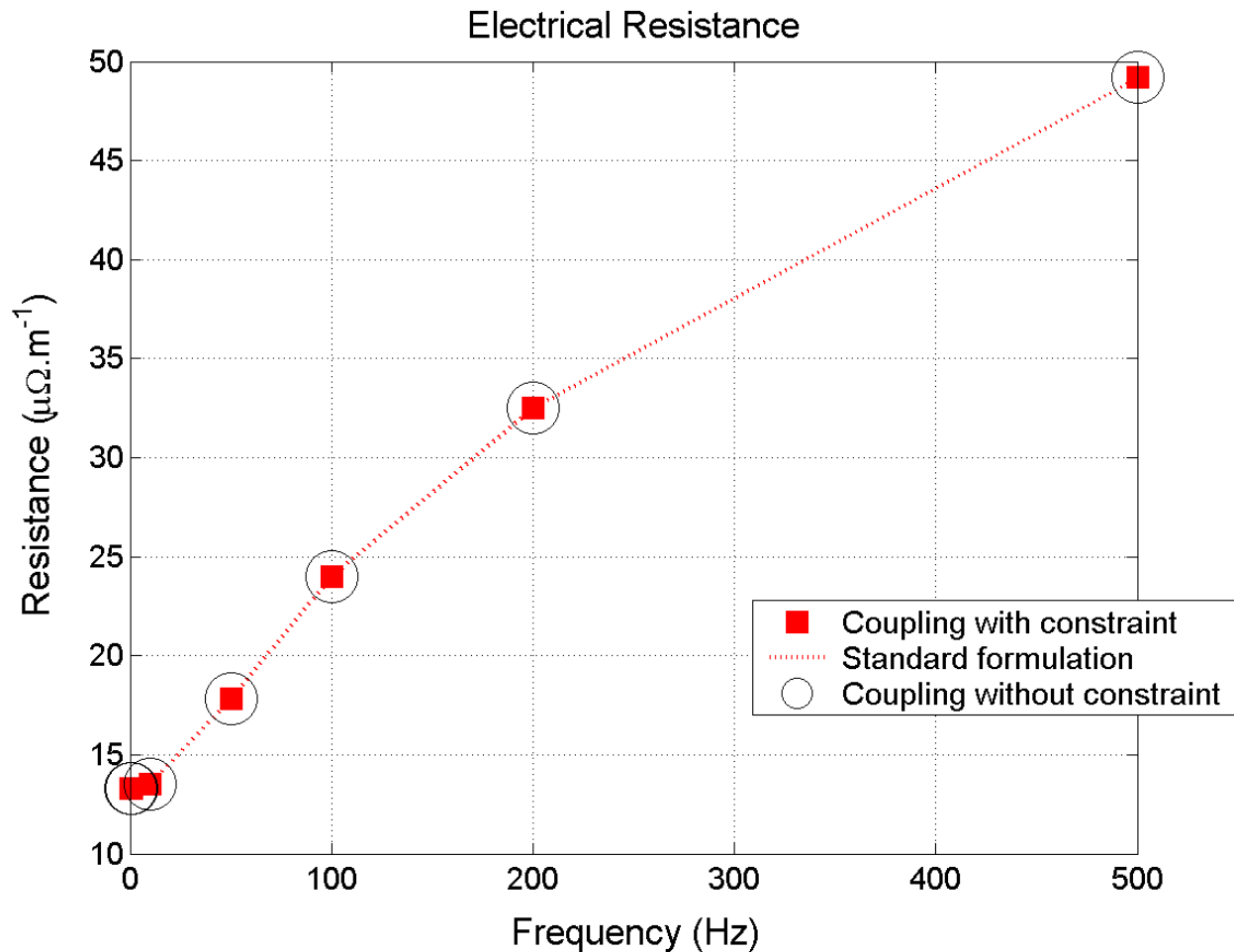
- Current-Voltage behaviour @ 50 Hz



3. Modelling of test cases

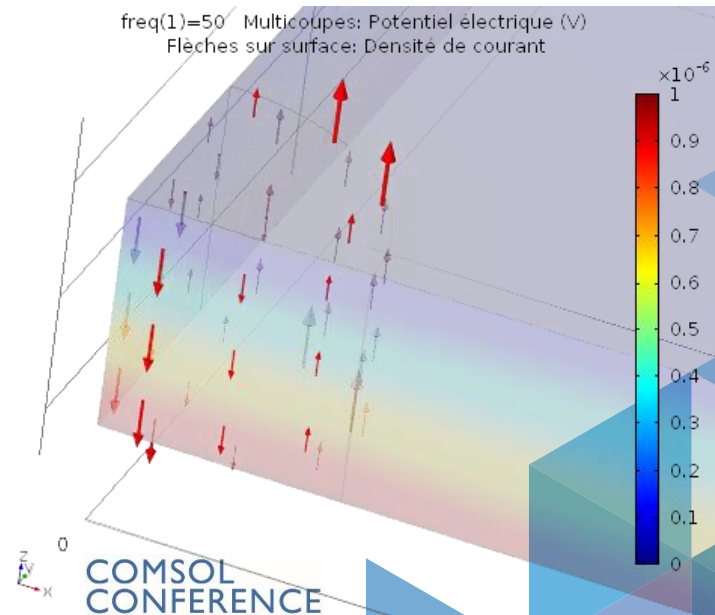
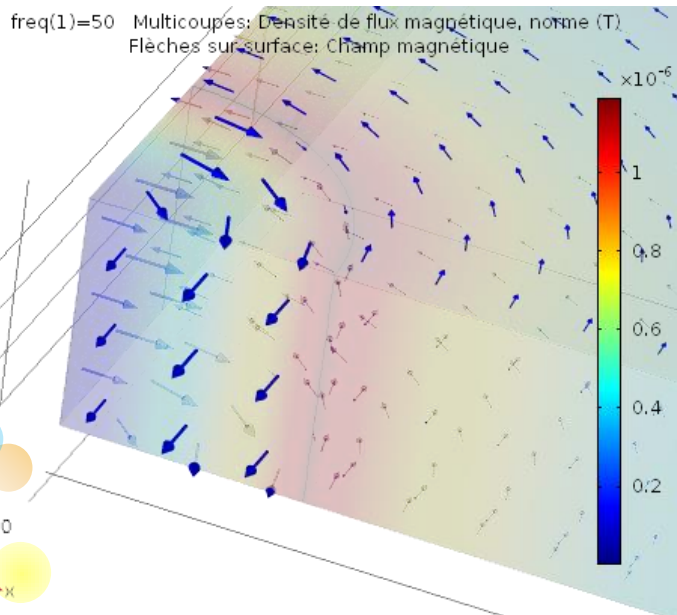
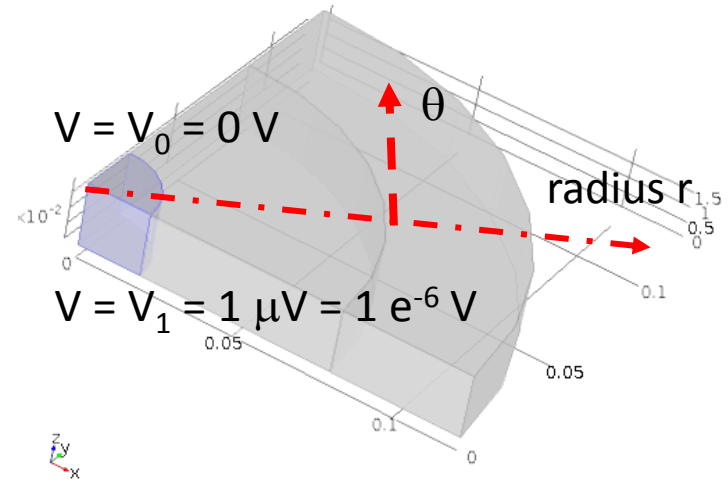
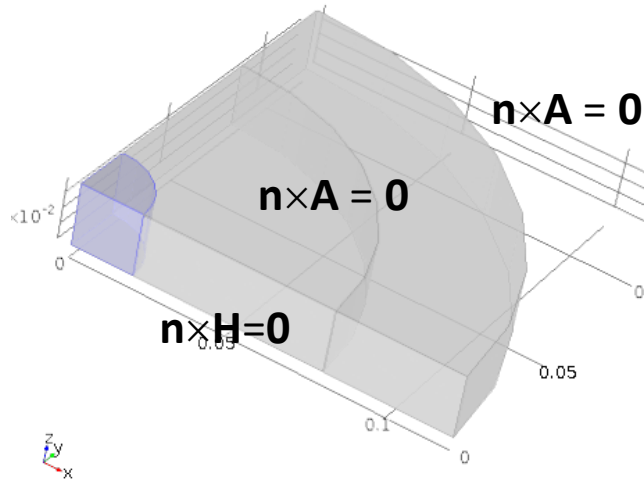
3.1. Test case 1 - *the wire*

- Equivalent resistance per unit length



3. Modelling of test cases

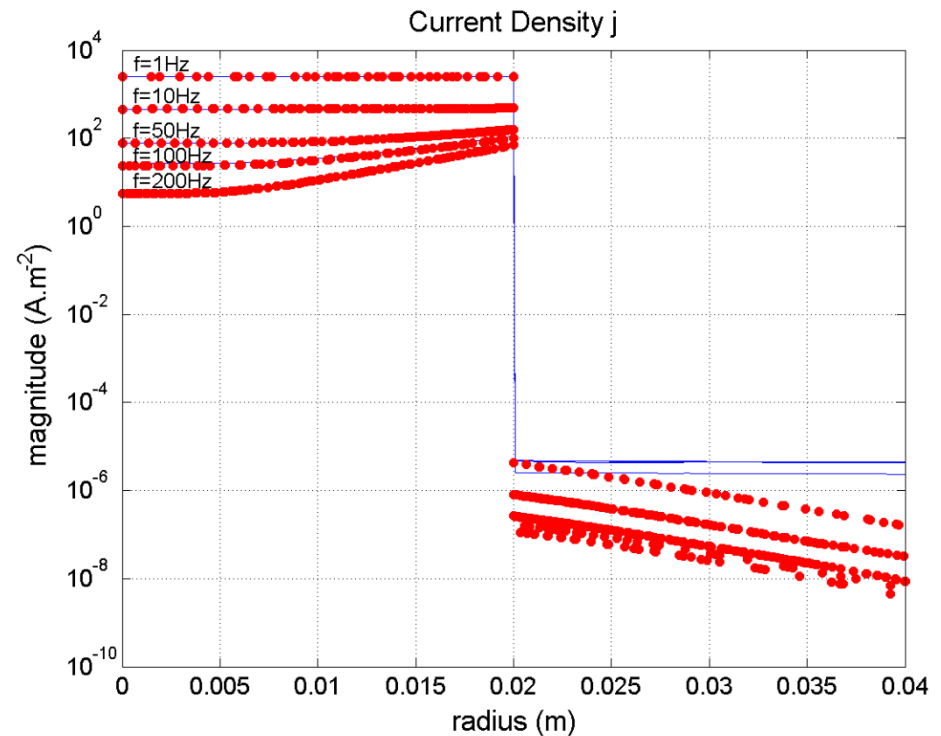
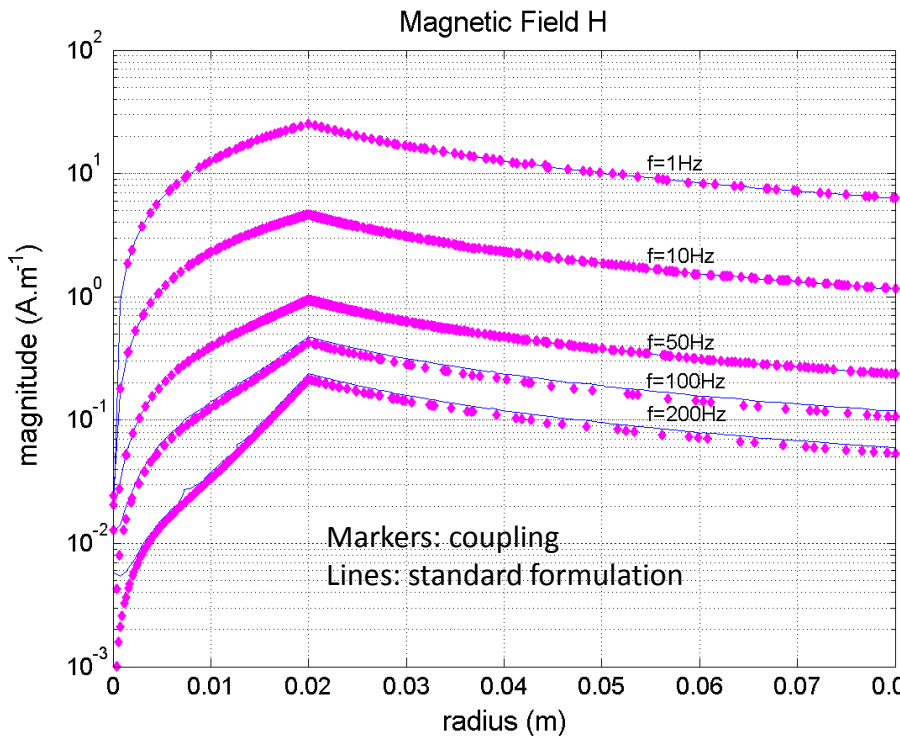
3.2. Test case 2 – *the wire in air*



3. Modelling of test cases

3.2. Test case 2 – *the wire in air*

- Field H and Current density j distribution

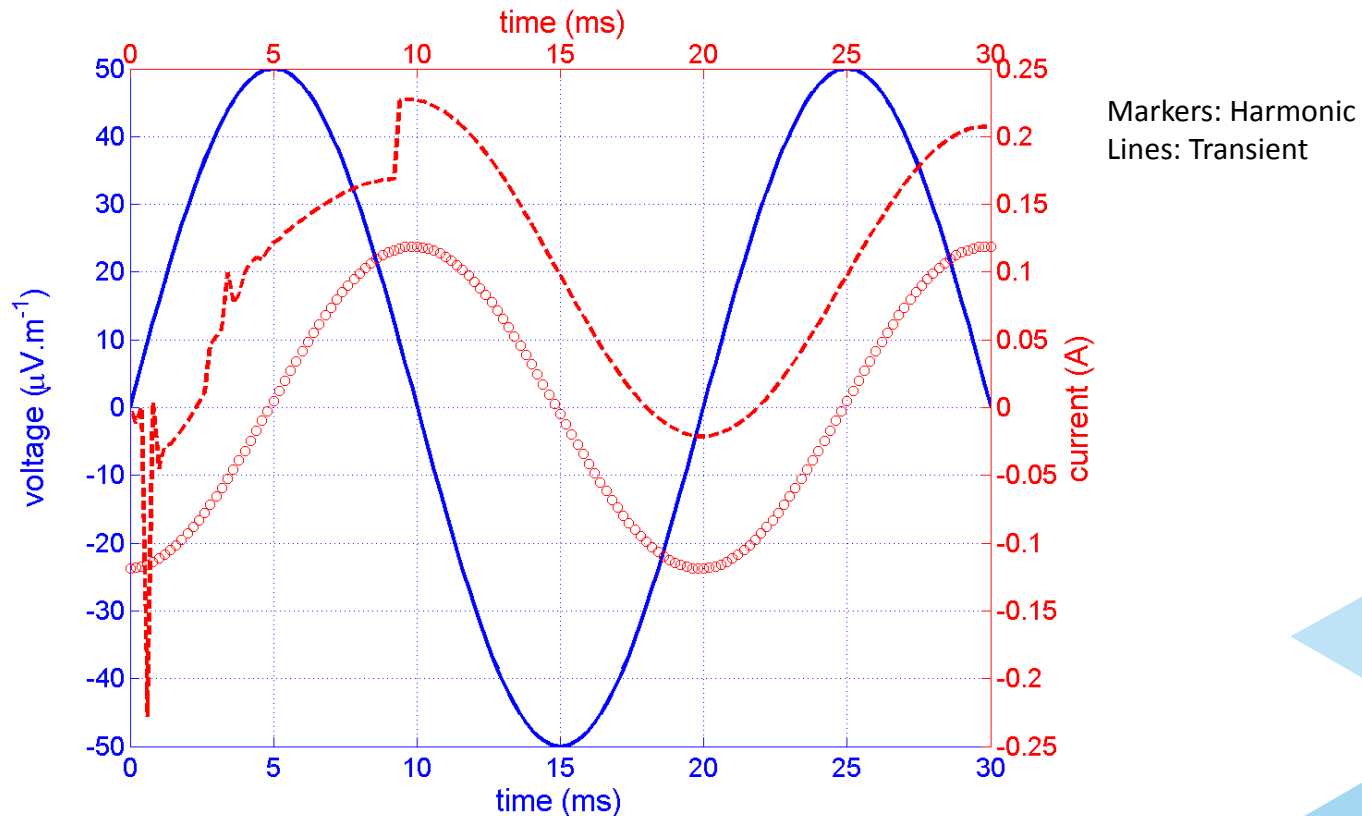


- Field damping due to both the inductance in air and eddy currents
- Eddy currents and skin effect correctly described
- Agreement between the two methods and formulations

3. Modelling of test cases

3.2. Test case 2 – *the wire in air*

- Harmonic vs transient behaviour @50 Hz

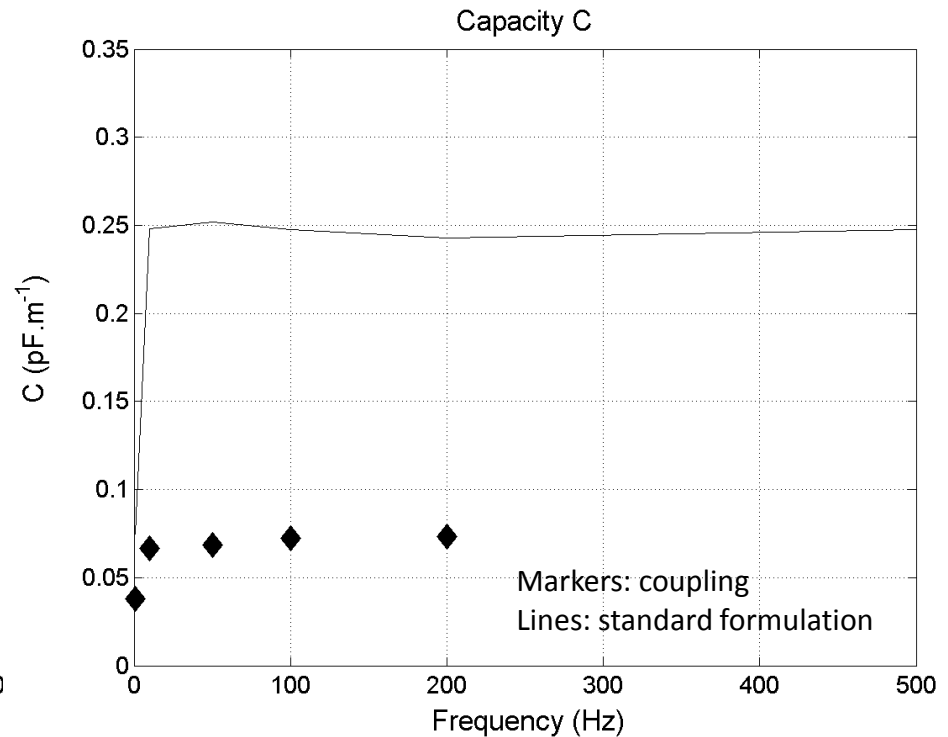
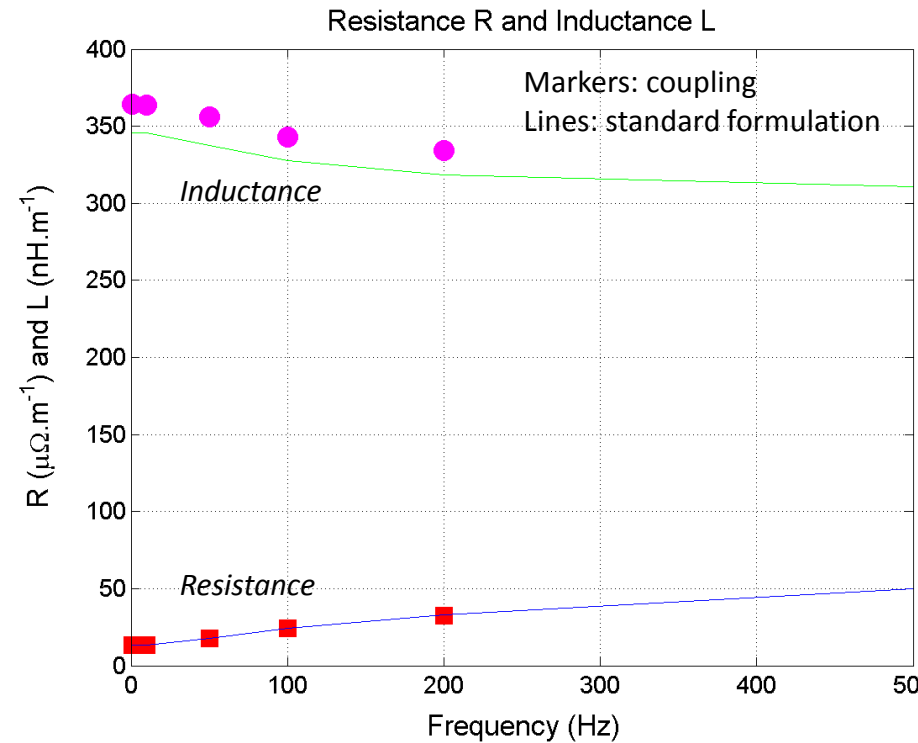


- Correct Magnitude and phase angle
- Wrong DC current (cause: Gauge? Convergence method?)

3. Modelling of test cases

3.2. Test case 2 - *the wire in air*

- Equivalent R, L and C per unit length



- Correct estimation of Resistance R and Inductance L
- Different Capacities C (cause: $\mathbf{E} = -\nabla V \neq \mathbf{E} = -\nabla V - \partial_t \mathbf{A}$)

4. Conclusion and Forthcomings

- **Conclusion:**

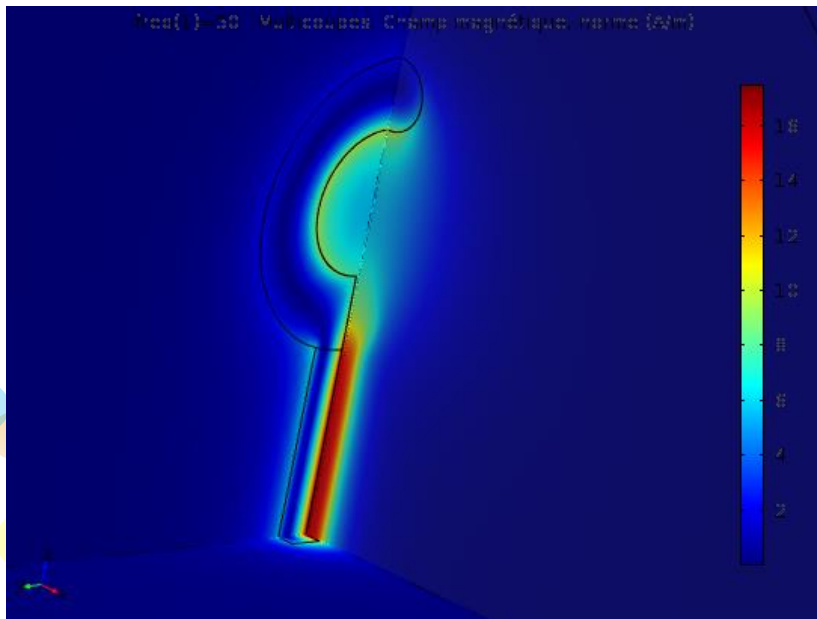
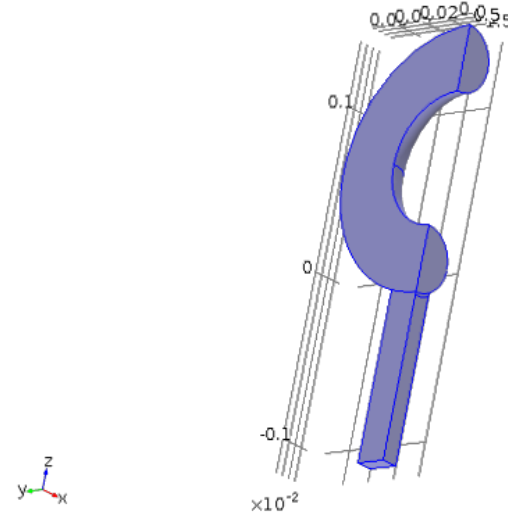
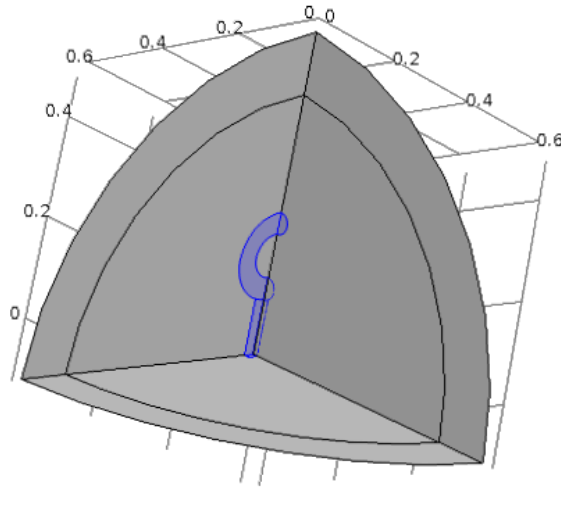
- (+) no geometry constraint on the coil
- (+) resistive, inductive and capacitive effects
- (+) transient working condition
- (-) big memory space needed
- (-) hard convergence
- (-) time consuming method

- **Forthcomings:**

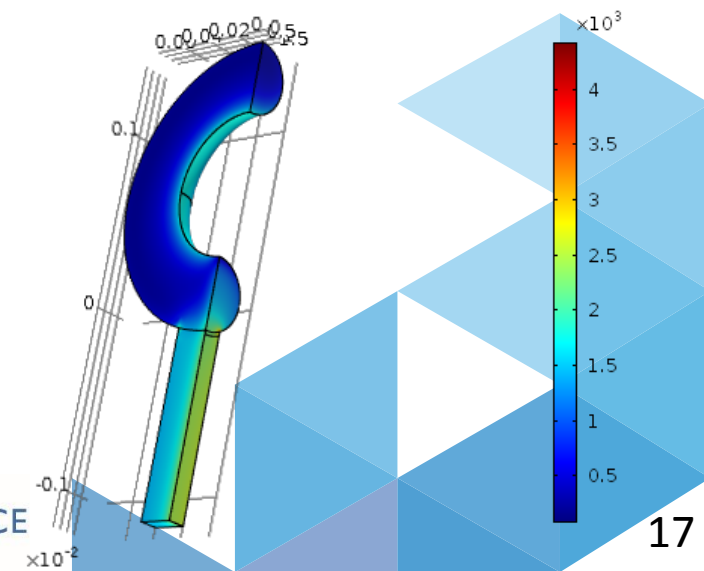
Apply the transient coupling formulation on the coil
Compare segregated and fully-coupled methods
Investigate other potentials formulations (\mathbf{T}, Φ)

3. Modelling of test cases

3.3. Test case 3 - *the coil*



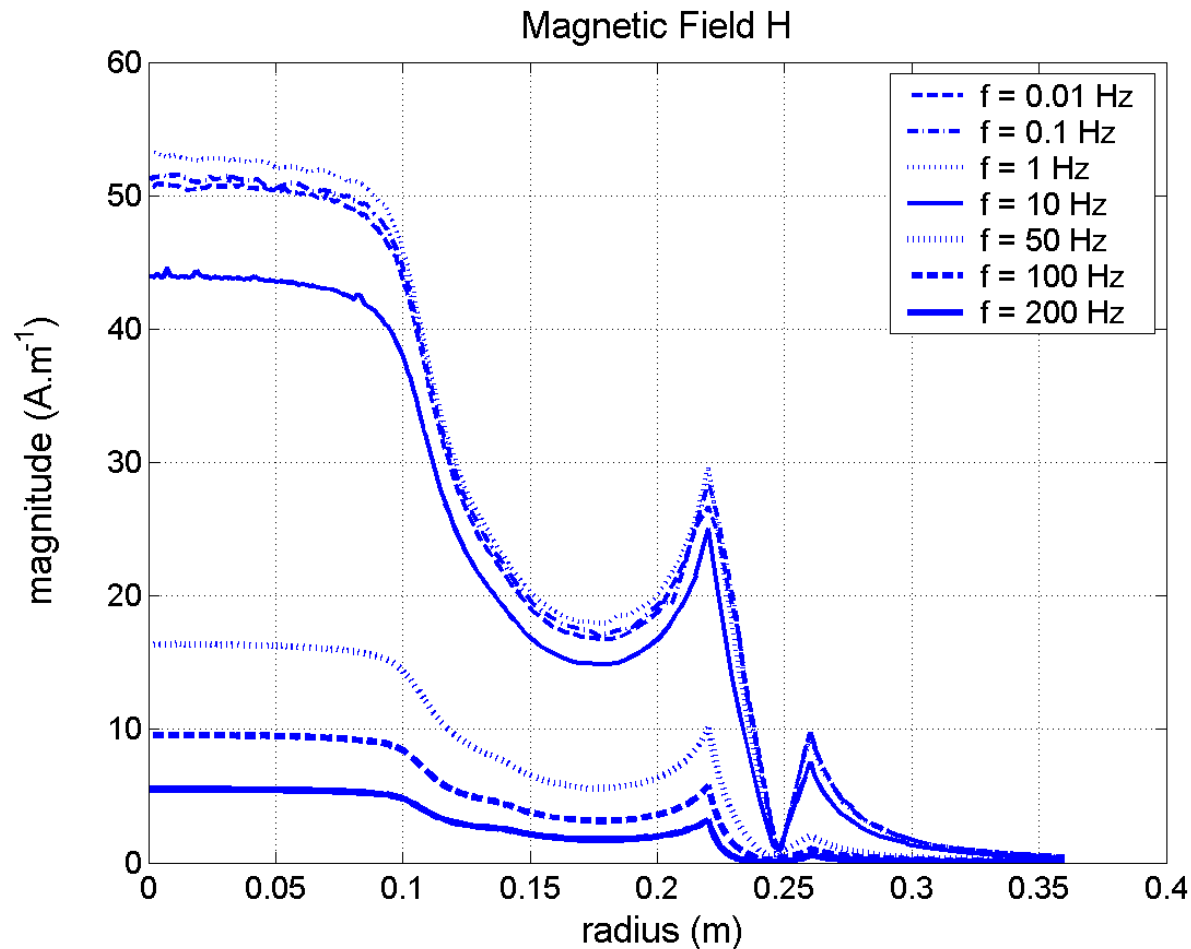
)=50 Volume: Densité de courant, norme (A/m²)



3. Modelling of test cases

3.3. Test case 3 - *the coil*

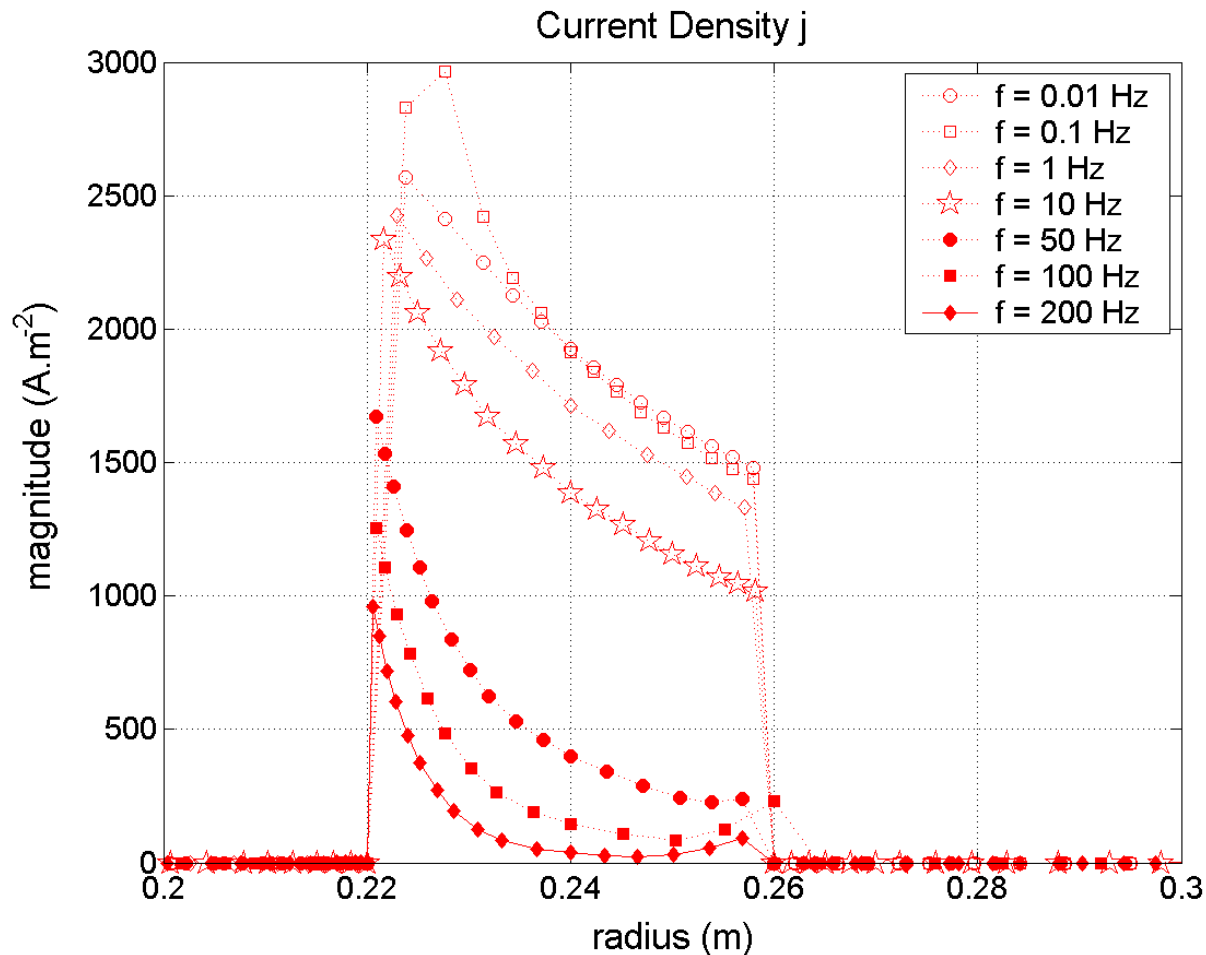
- Field distribution



3. Modelling of test cases

3.3. Test case 3 - *the coil*

- Current distribution

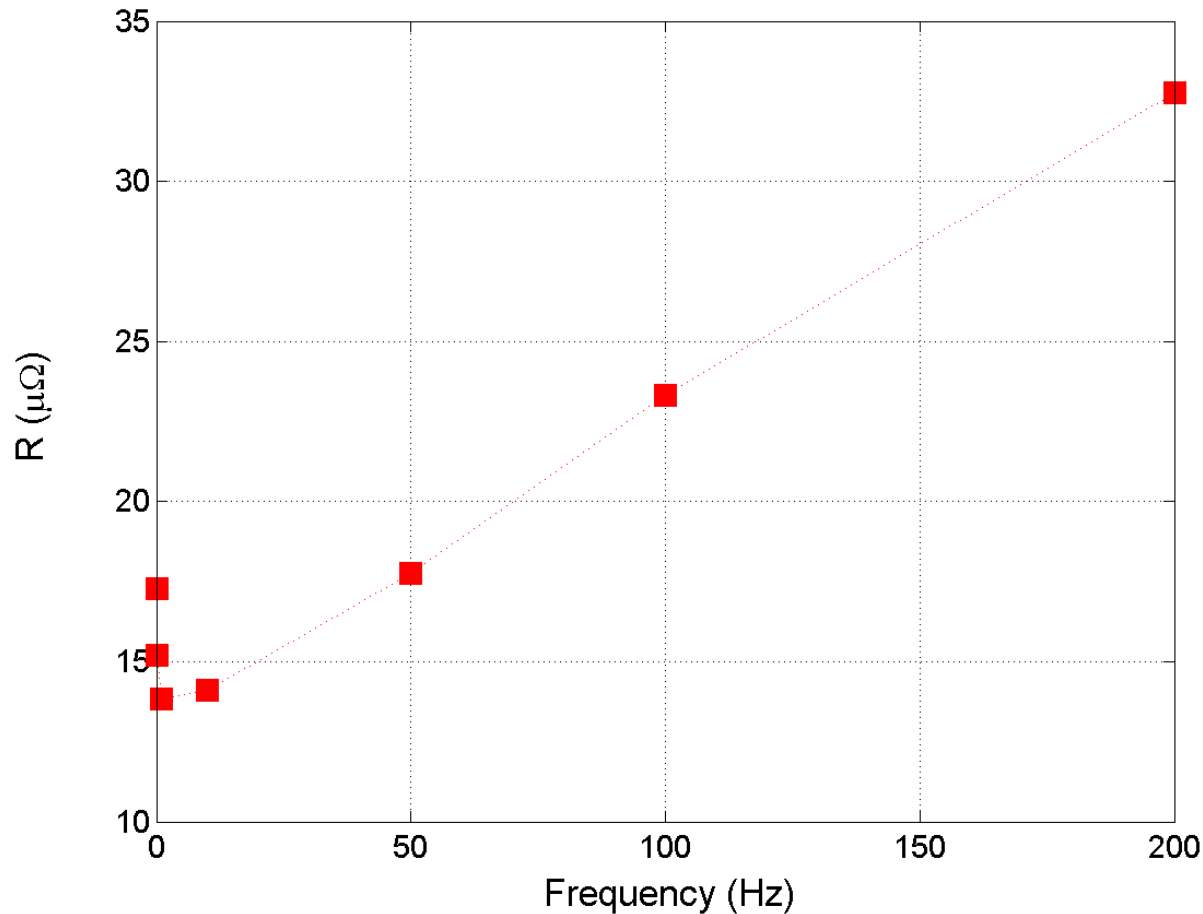


3. Modelling of test cases

3.3. Test case 3 - *the coil*

- Equivalent R, L and C per unit length

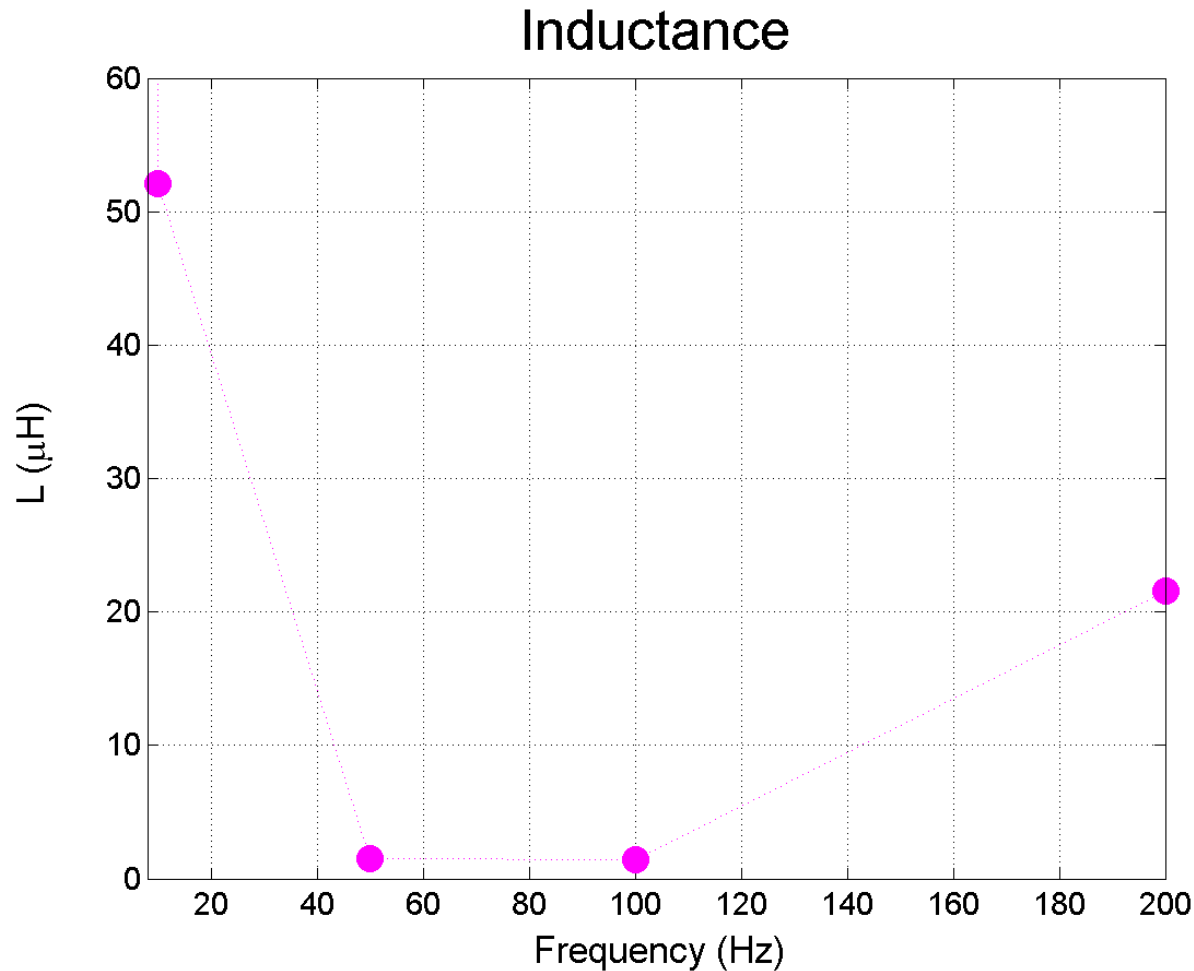
Resistance R



3. Modelling of test cases

3.3. Test case 3 - *the coil*

- Equivalent R, L and C per unit length



3. Modelling of test cases

3.3. Test case 3 - *the coil*

- Equivalent R, L and C per unit length

